

Comparison of cell-centered and node-centered formulations of a high-resolution well-balanced finite volume scheme: application to shallow water flows

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By the words of Morton and Sonar (Acta Numerica, 2007):

**"The jury was out there for a long time in the judgment between cell-center
and vertex-center methods"**



Overview

→ The 2D nonlinear shallow water model



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- The Malpasset dam case
- Conclusions



MATHEMATICAL MODEL: 2D Non-linear Shallow Water Equations

$$\frac{\partial \mathbf{U}}{\partial t} + \nabla \cdot \mathcal{F}(\mathbf{U}) = \mathcal{L}(\mathbf{U}, x, y) \quad \text{on} \quad \Omega \times [0, t] \subset \mathbb{R}^2 \times \mathbb{R}^+,$$

$$\mathbf{U} = \begin{bmatrix} h \\ hu \\ hv \end{bmatrix}, \quad \mathcal{F}(\mathbf{U}) = [\mathbf{F} \quad \mathbf{G}] = \begin{bmatrix} hu & hv \\ hu^2 + \frac{1}{2}gh^2 & huv \\ huv & hv^2 + \frac{1}{2}gh^2 \end{bmatrix},$$

$$\mathcal{L}(\mathbf{U}) = [\mathbf{R}^1 + \mathbf{R}^2 + \mathbf{S}]$$
$$\mathbf{R}^1 = \begin{bmatrix} 0 & -gh \frac{\partial B(x,y)}{\partial x} & 0 \end{bmatrix}^T \quad \text{and} \quad \mathbf{R}^2 = \begin{bmatrix} 0 & 0 & -gh \frac{\partial B(x,y)}{\partial y} \end{bmatrix}^T \quad \text{and}$$

$$\mathbf{S} = \begin{bmatrix} 0 & -gh S_f^x & -gh S_f^y \end{bmatrix}^T,$$

$$S_f^x = n_m^2 \frac{u \sqrt{u^2 + v^2}}{h^{4/3}}, \quad S_f^y = n_m^2 \frac{v \sqrt{u^2 + v^2}}{h^{4/3}}$$



Constructing Numerical Methods: Objectives

We need numerical schemes that are:

1. Conservative (conservation of physical quantities).



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7. Enable various practical inflow/outflow boundary conditions



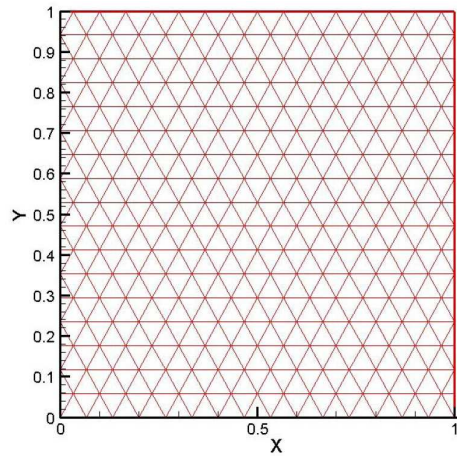
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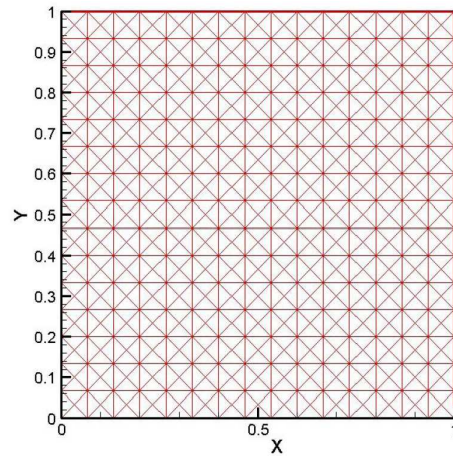
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7. Enable various practical inflow/outflow boundary conditions
8. Preserve the positivity of the water depth.



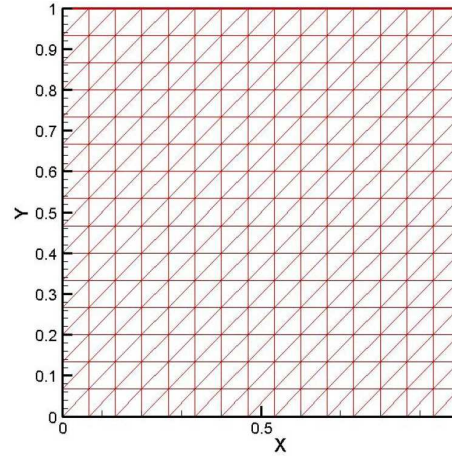
Grid Terminology



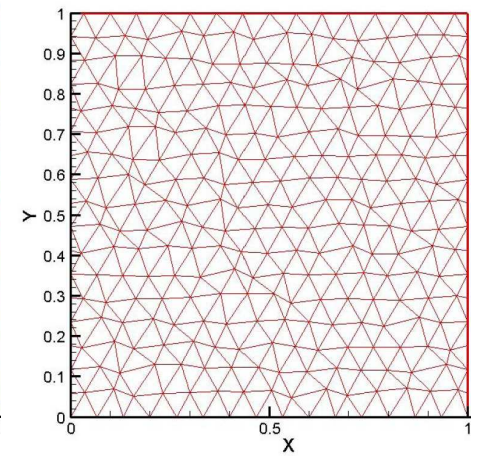
(a) Equilateral (Type-I)



(b) Orthogonal (Type-II)

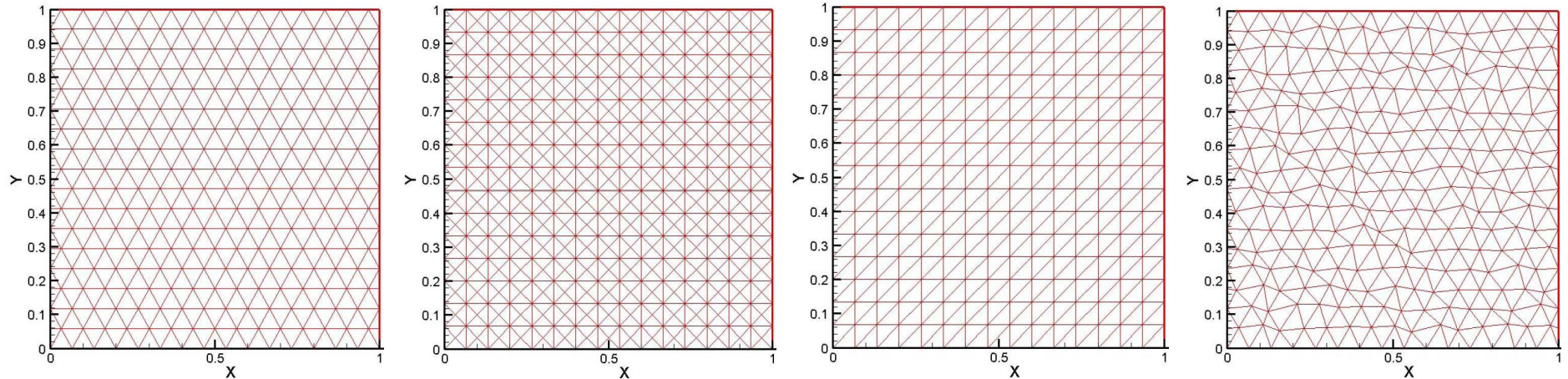


(c) Orthogonal (Type-III)



(d) Distorted (Type-IV)

Grid Terminology

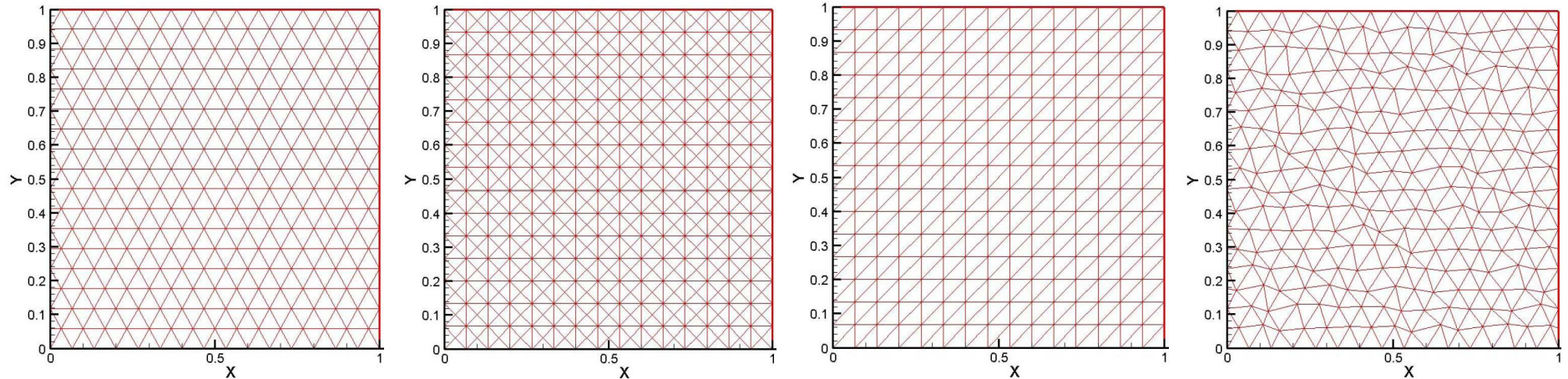


(a) Equilateral (Type-I) (b) Orthogonal (Type-II) (c) Orthogonal (Type-III) (d) Distorted (Type-IV)

→ Major requirement: to enable meaningful asymptotic order of convergence use **consistently refined grids**, i.e. for $N =$ degrees of freedom, the characteristic length $h_N = \sqrt{(L_x \times L_y)/N}$,



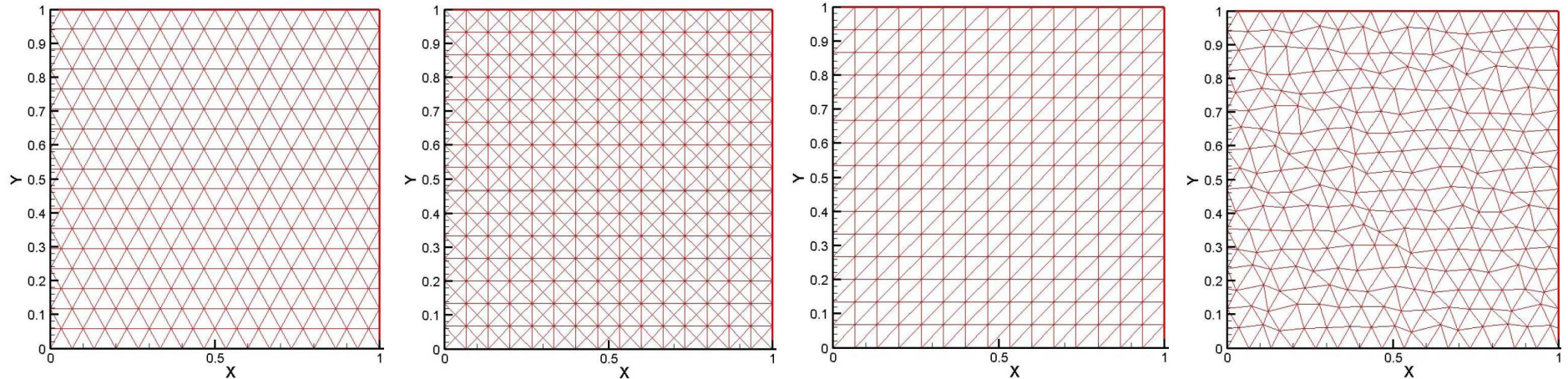
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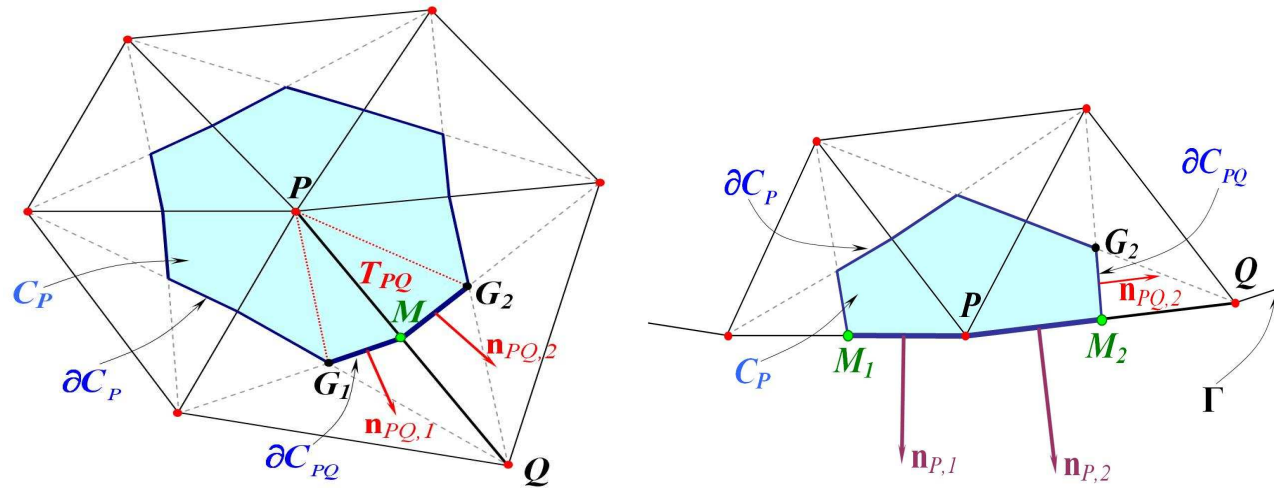


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- For fair comparison between NCFV and CCFV need to derive **equivalent meshes**, based on the degrees of freedom N ,
- Measure the grid irregularity, e.g. use proper grid metrics.

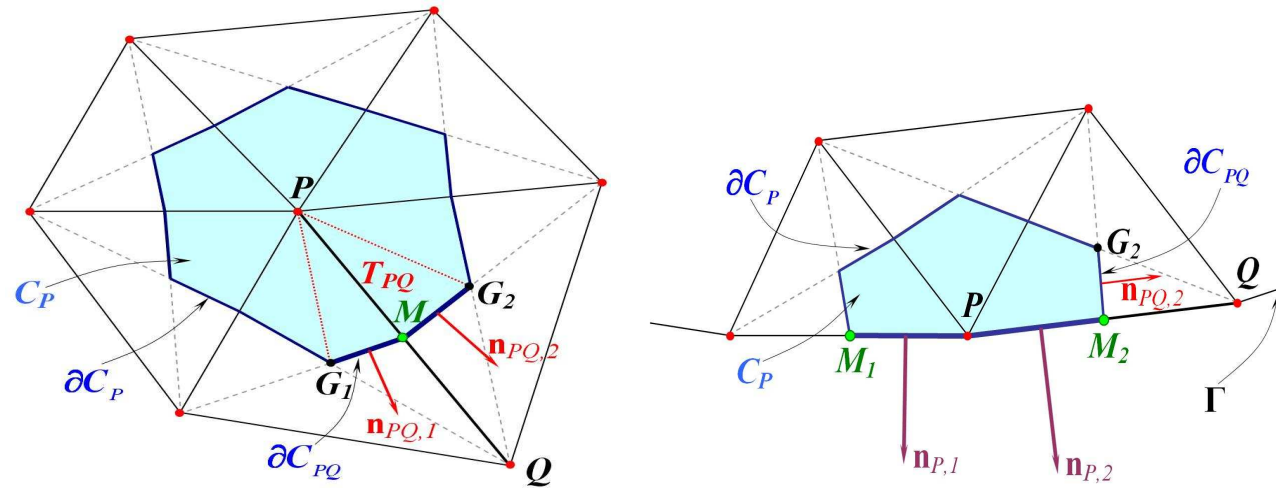


FV discretization schemes on triangles: NCFV approach



$$\iint_{C_P} \frac{\partial \mathbf{U}}{\partial t} dx dy + \oint_{\partial C_P} (\mathbf{F} \tilde{n}_x + \mathbf{G} \tilde{n}_y) dl = \iint_{C_P} \mathcal{L} dx dy$$

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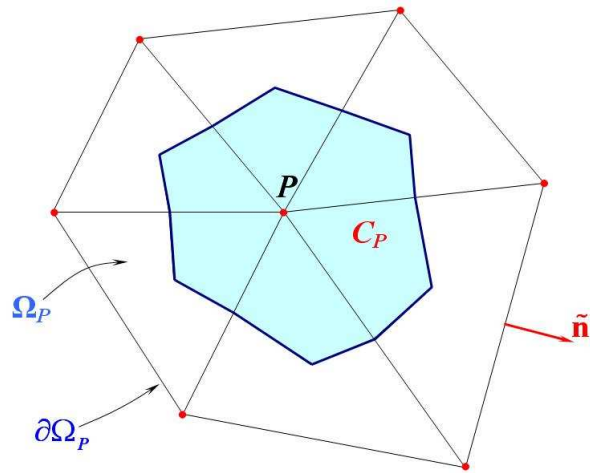
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$$\frac{\partial \mathbf{U}_P}{\partial t} |C_P| + \sum_{Q \in K_P} \Phi_{PQ} + \Phi_{P,out} = \sum_{Q \in K_P} \left\{ \iint_{T_{PQ}} \mathcal{L} dx dy \right\} \quad \text{where}$$

$$\Phi_{PQ} = \mathbf{Z} \left(\mathbf{U}_{PQ}^L, \mathbf{n}_{PQ} \right) + \tilde{\mathbf{J}}_{PQ}^- \left(\mathbf{U}_{PQ}^R - \mathbf{U}_{PQ}^L \right), \quad \text{with} \quad \tilde{\mathbf{J}}_{PQ}^- = \left(\tilde{\mathbf{P}} \tilde{\Lambda} - \tilde{\mathbf{P}}^{-1} \right)_{PQ},$$

Φ_{PQ} is the **Roe numerical flux**, evaluated at \mathbf{U}_{PQ}^L and \mathbf{U}_{PQ}^R **reconstructed values**.

For MUSCL $(\nabla \mathbf{W})_P$ has to be computed in each dual cell P



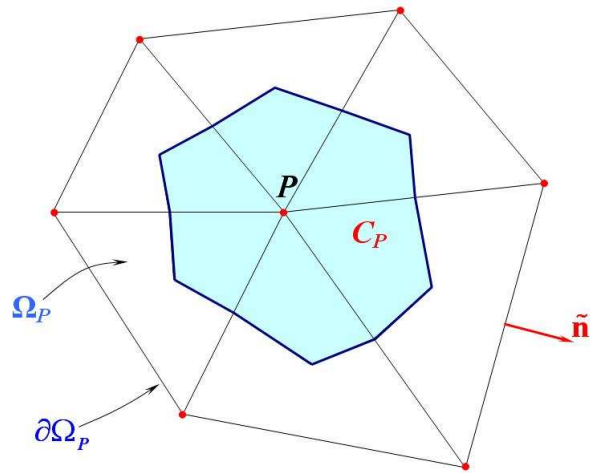
Green-Gauss (G-G) linear reconstruction

$$(\nabla w_i)_P = \frac{1}{|C_P|} \sum_{Q \in K_P} \frac{1}{2} (w_{i,P} + w_{i,Q}) \mathbf{n}_{PQ}.$$

$$w_{i,PQ}^L = w_{i,P} + \frac{1}{2} \text{LIM} \left((\nabla w_i)_P^{\text{upw}} \cdot \mathbf{r}_{PQ}, (\nabla w_i)^{\text{cent}} \cdot \mathbf{r}_{PQ} \right);$$

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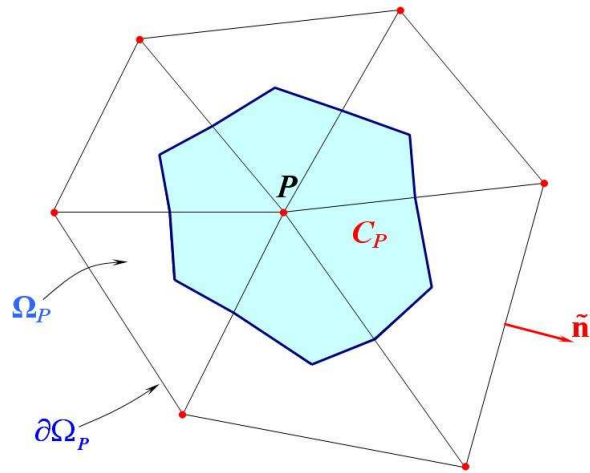
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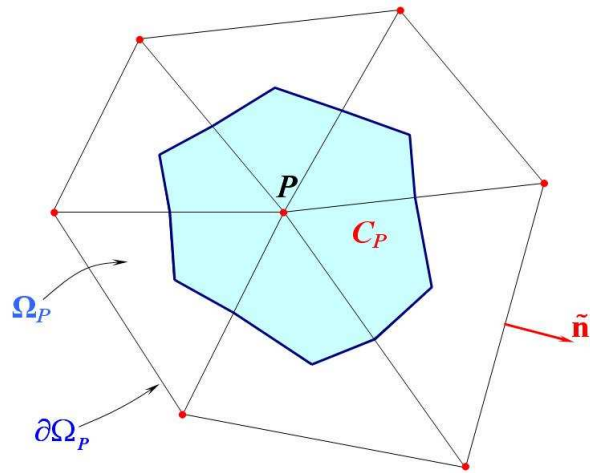
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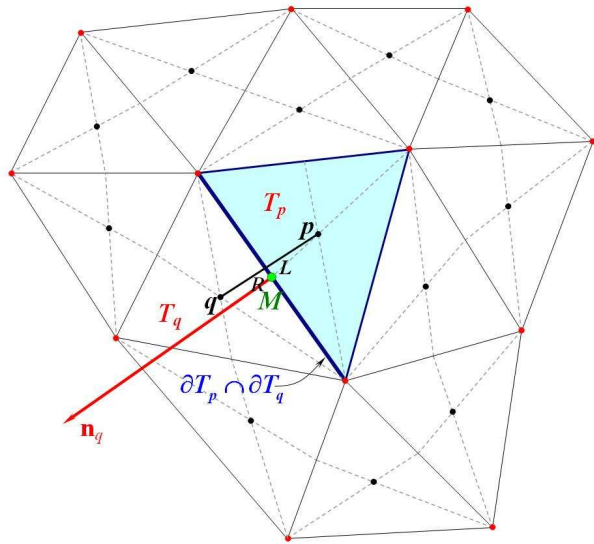
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- The same reconstruction is used to compute the gradient for $B(x, y)$.



FV discretization schemes on triangles: CCFV approach

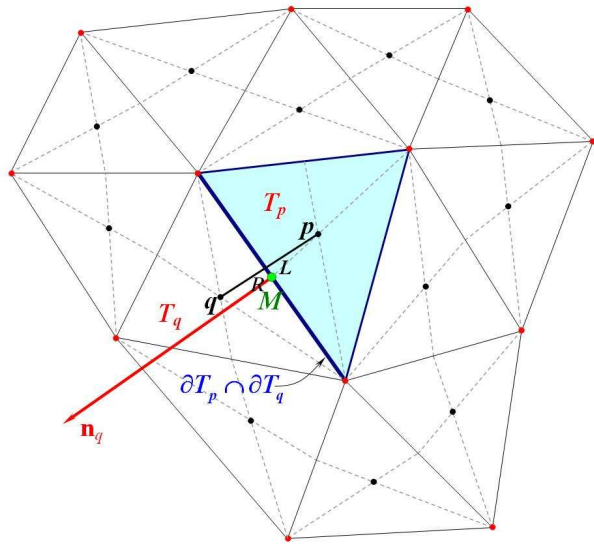


$$\frac{\partial \mathbf{U}_p}{\partial t} |T_p| = \sum_{q \in K(p)} \Phi_q + \iint_{T_p} \mathcal{L} d\Omega.$$

With the usual one point quadrature at M , Roe's solver is again utilized

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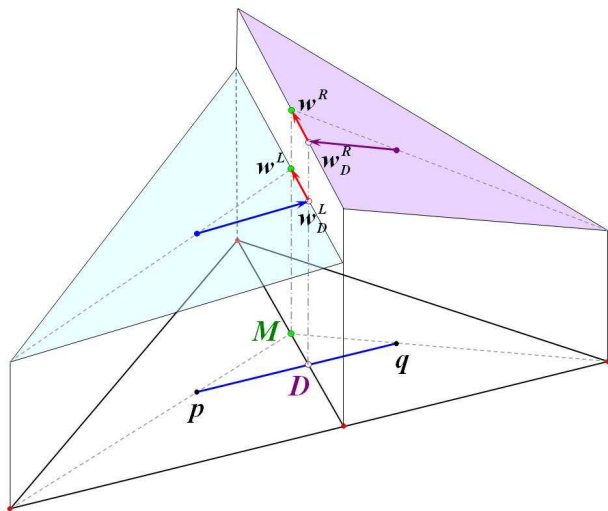
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Linear reconstruction for the CCFV scheme

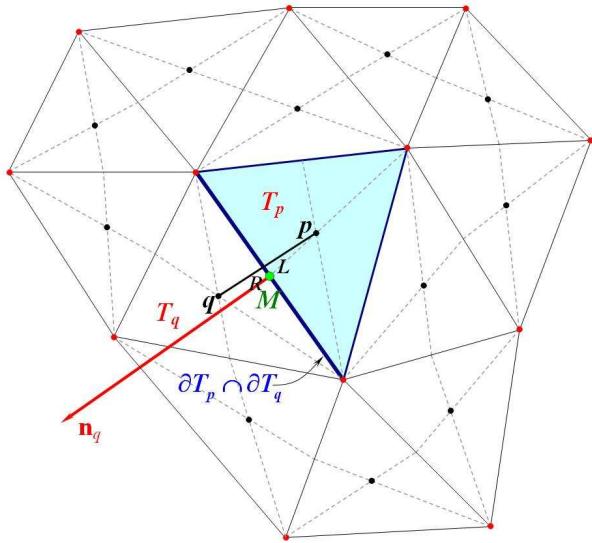
- Naive calculation (at point D)

$$(w_{i,p})_D^L = w_{i,p} + \frac{\|\mathbf{r}_{pD}\|}{\|\mathbf{r}_{pq}\|} \text{LIM} \left((\nabla w_i)_p^{\text{upw}} \cdot \mathbf{r}_{pq}, (\nabla w_i)^{\text{cent}} \cdot \mathbf{r}_{pq} \right);$$

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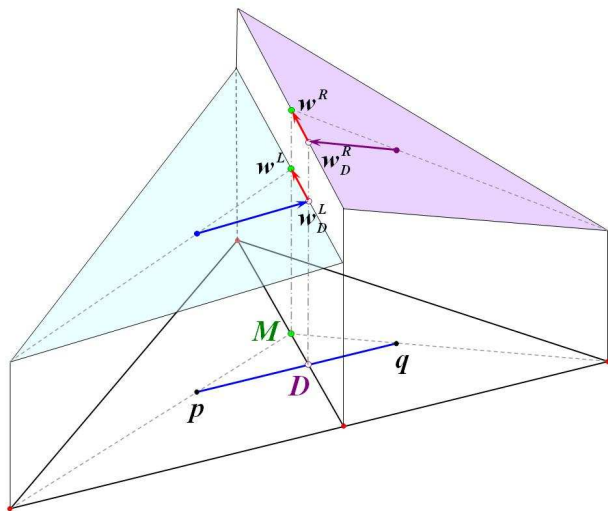
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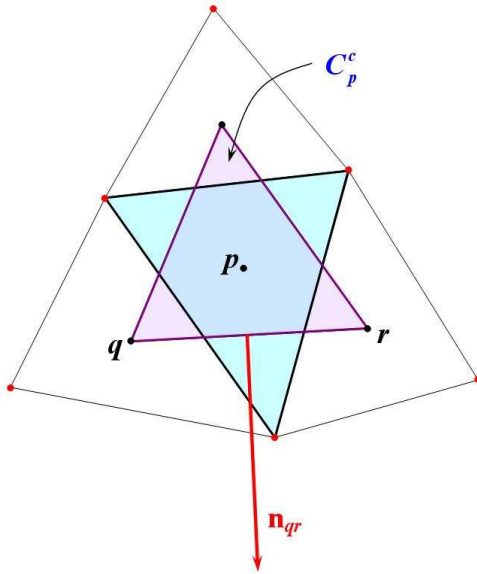
- Corrected calculation (at point M)

$$w_{i,p}^L = (w_{i,p})_D^L + \mathbf{r}_{DM} \cdot (\nabla w_i)_p,$$

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CCFV approach: Gradient operators



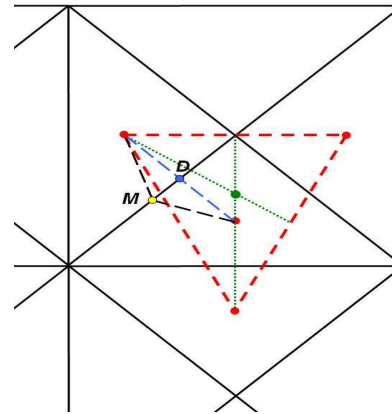
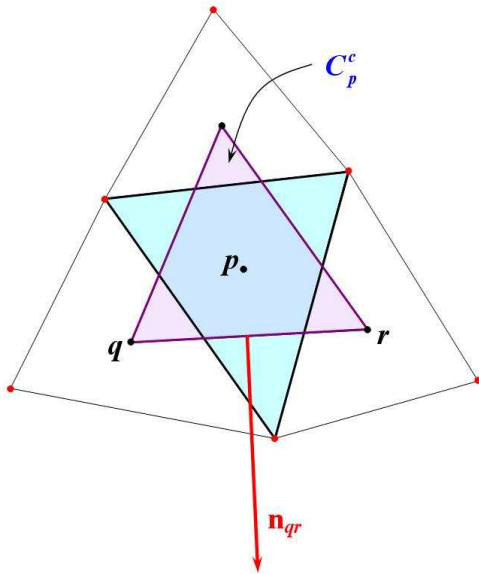
Three element (compact stencil) gradient

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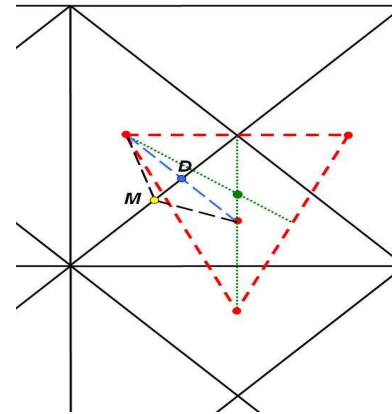
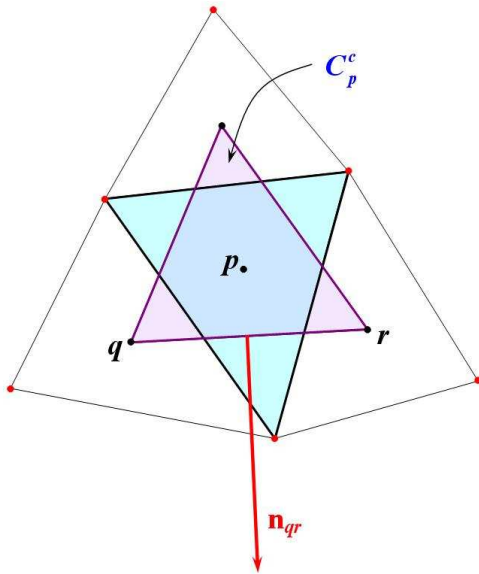
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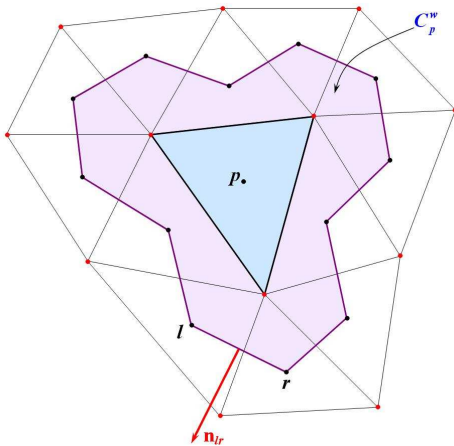
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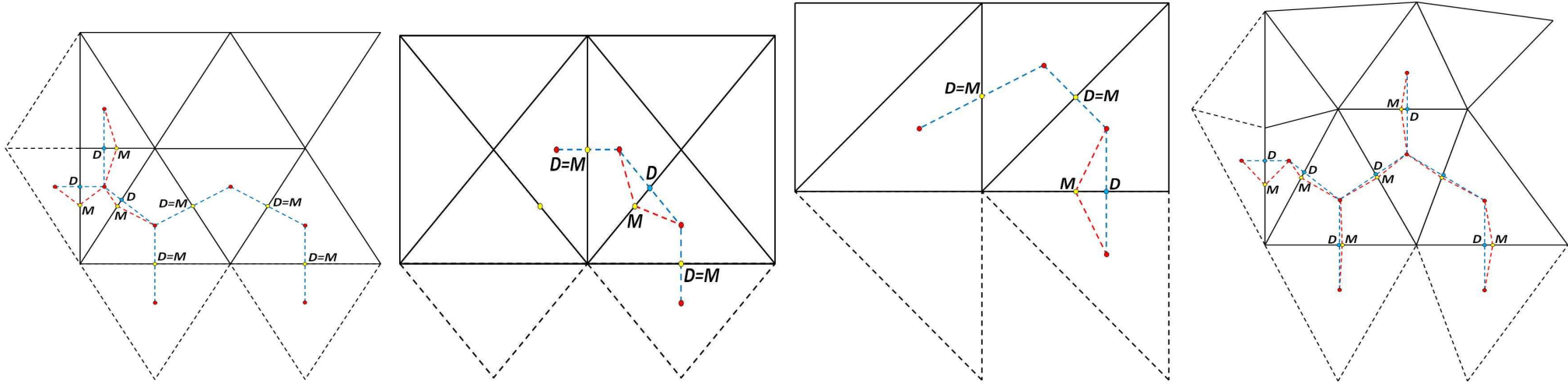


Extended element (wide stencil) gradient

$$\nabla w_{i,p} = \frac{1}{|C_p^w|} \sum_{\substack{l,r \in K'(p) \\ r \neq l}} \frac{1}{2} (w_{i,l} + w_{i,r}) \mathbf{n}_{lr}$$



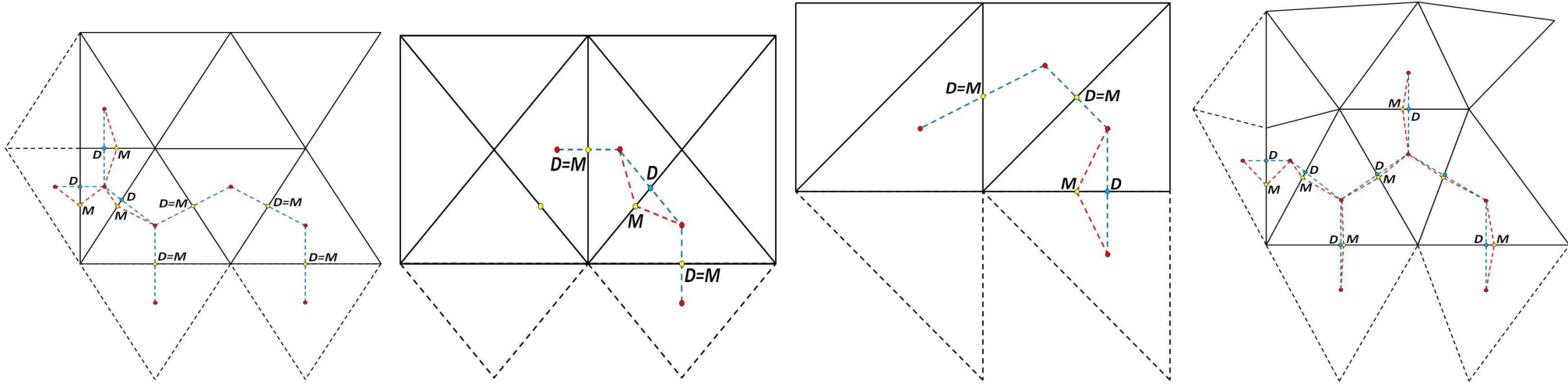
Typical behavior of the CCFV scheme at internal and boundary faces



- Keeping in mind that, we want to apply the same edge-based limiter as for the NCFV scheme

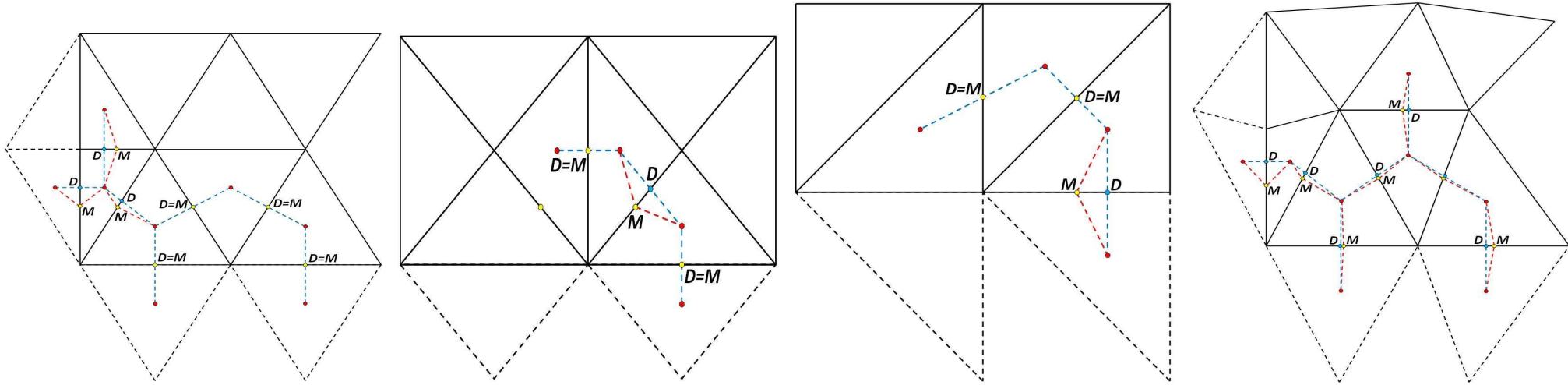


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- In an ideal unstructured grid, variables are extrapolated at M which will coincide with D (intersection point of face $\partial T_q \cap \partial T_p$ and \overline{pq}).
- There can be a "large" distance between M and D (also on boundary faces, where ghost cells are used).

Topography source discretization (wet/wet case)

→ **C-property:** (Bermudez and Vazquez, 1994)

A numerical should resolve exactly steady-state cases where:

$$u = v \equiv 0, \quad B^R - B^L = -(h^R - h^L).$$



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→ Upwind of the numerical source contribution to cell- i as

$$\tilde{\Psi}^- = \frac{1}{2} \left(\tilde{\mathbf{P}} \left(\mathbf{I} - \left| \tilde{\Lambda} \right| \tilde{\Lambda}^{-1} \right) \tilde{\mathbf{P}}^{-1} \tilde{\mathbf{R}} \right)$$



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But what about wet/dry fronts and flow over adverse slopes?



Topography source discretization (wet/dry case)

→ **Extended C-property**, (Castro et al., 2005)

A scheme is considered to be well-balanced if it can solve exactly steady-state solutions corresponding to flow at rest, regardless of including wet/dry transitions or not.

→ In the MUSCL scheme for hydrostatic conditions we must have, at i -cell



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→ For emerging bed situations, in the dry i -node (cell), the bed value has to be redefined (Brufau et al., 2002) in $\tilde{\mathbf{R}}$ and in order to maintain hydrostatic conditions i.e.

$$\Delta B = \begin{cases} -(h^R - h^L), & \text{if } h^L > \varepsilon_{wd}, h^R \leq \varepsilon_{wd} \text{ and } h^R < (B^R - B^L), \\ (B^L - B^R), & \text{otherwise.} \end{cases}$$



Solving at wet/dry front interface (continued)

For water in motion over emerging slopes, (Castro et al., 2005)

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→ Finally in case of steep downhill slopes, h in wet cells may become negative. We apply the conservative approach of Brufau et. al. (2004) to **control negative depths and conserve mass.**



Other implementation details:

- **Dry cell identification:** use a wet/dry tolerance parameter ε_{wd} depending on grid characteristics (Ricchiuto and Bollerman, 2009).

$$\varepsilon_{wd} = \left(\frac{h_N}{L^{ref}} \right)^2$$



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- Apply a four stage **2nd order Runge-Kutta scheme**, due to its enhanced stability region, under the CFL condition

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- Semi-implicit or implicit treatment for the **friction source** term within each cell following Brufau et al., 2004 and Serrano-Pacheco et al., 2009.



NUMERICAL RESULTS and COMPARISONS

Scheme	Description
NCFV	Node-Centered FV Scheme
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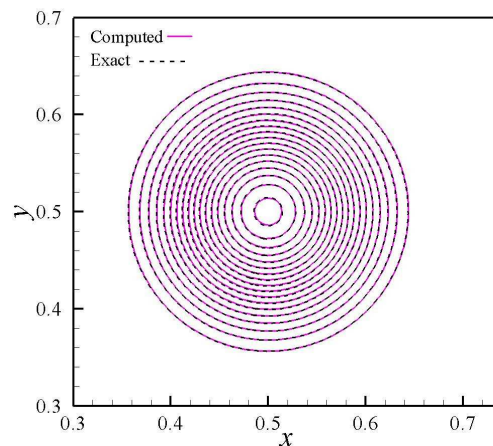
A traveling vortex solution (with periodic boundary conditions)



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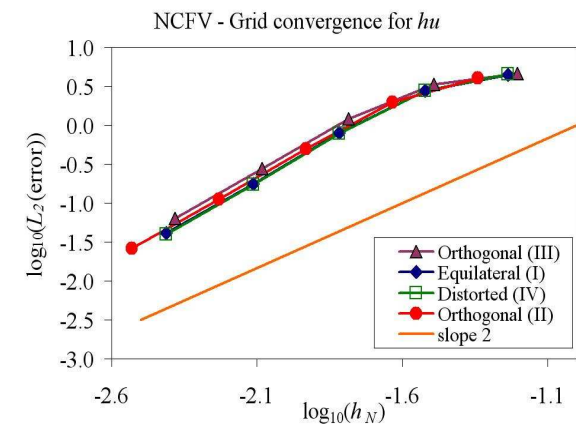
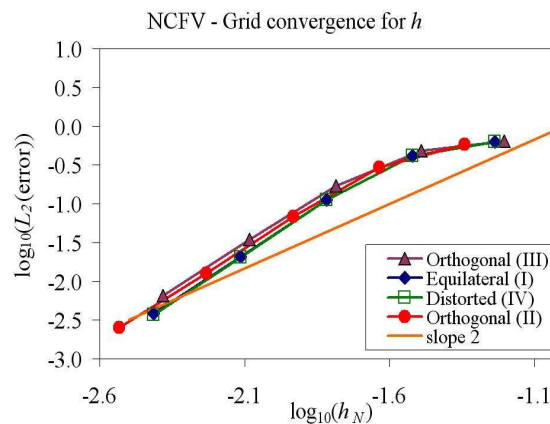
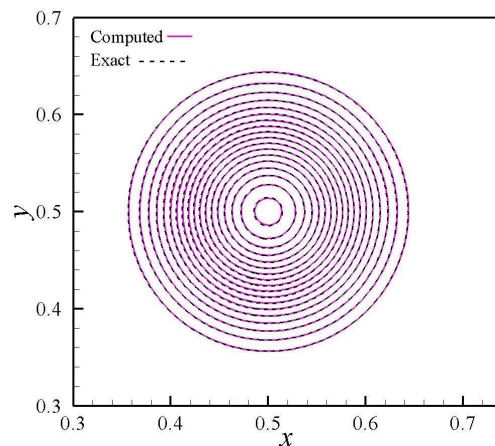
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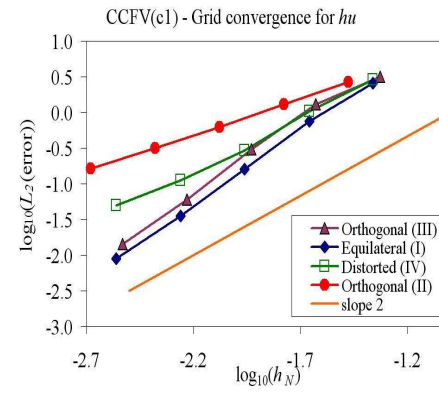
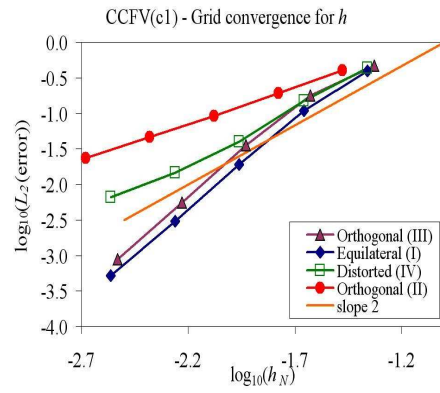
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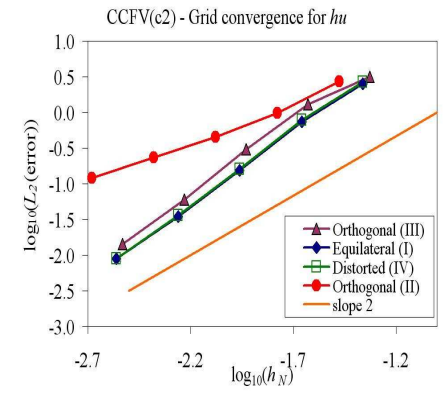
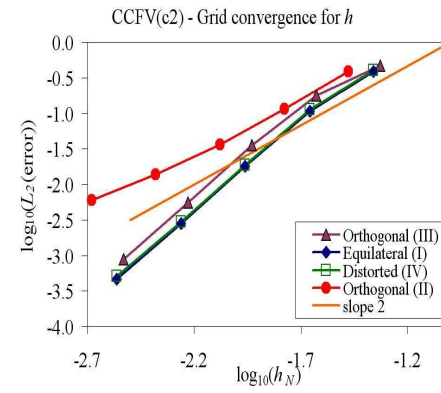
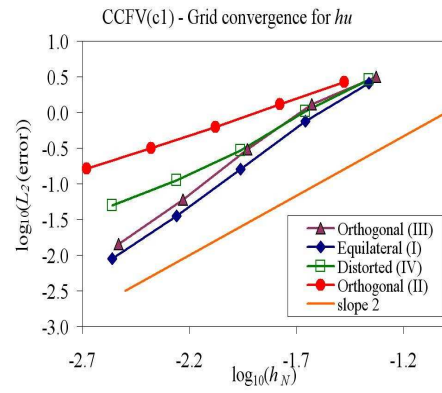
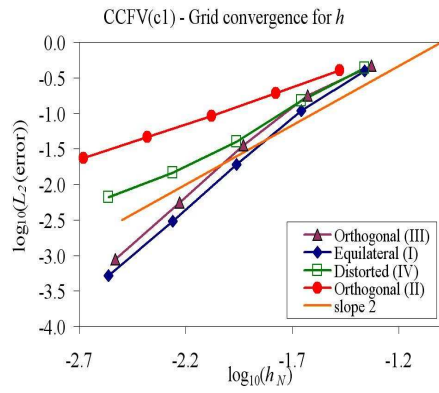
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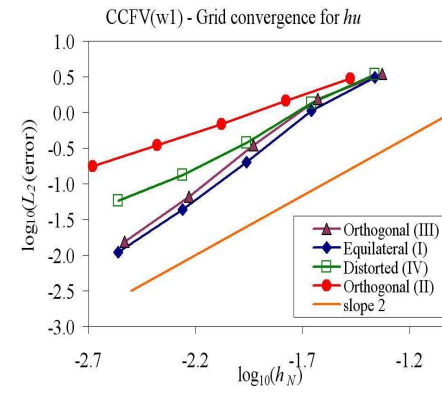
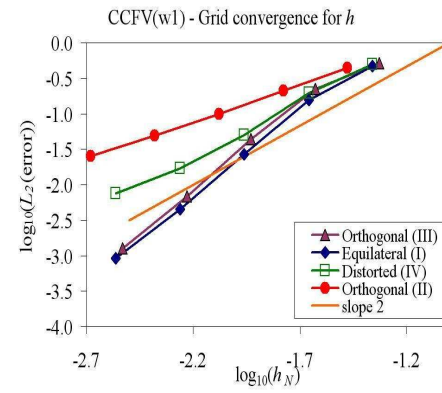
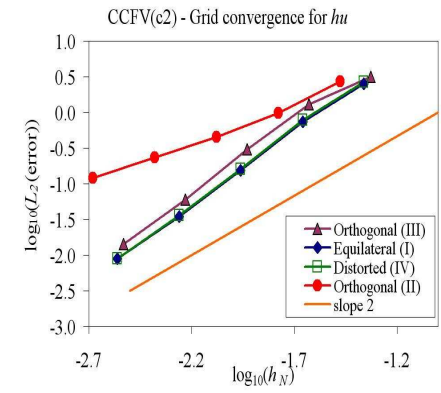
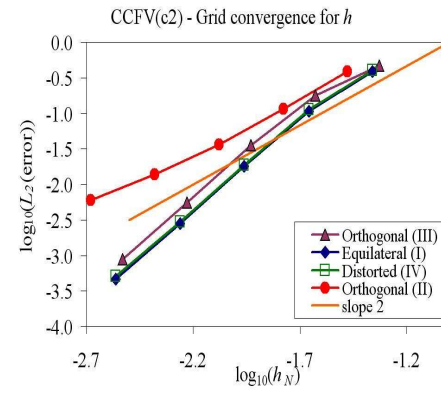
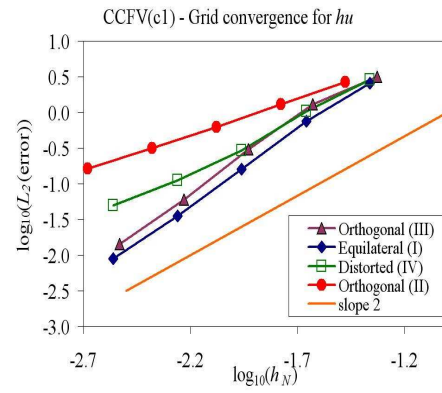
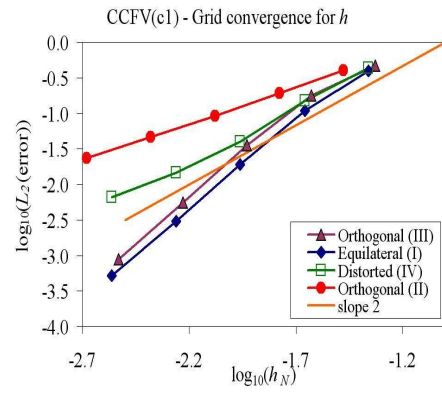
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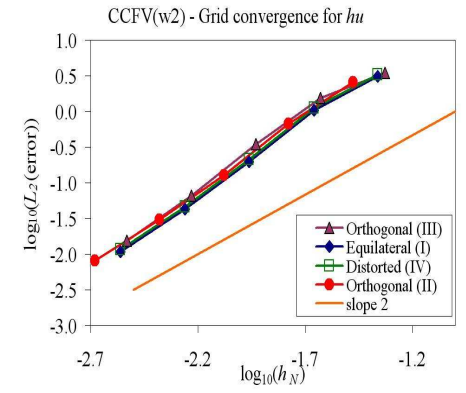
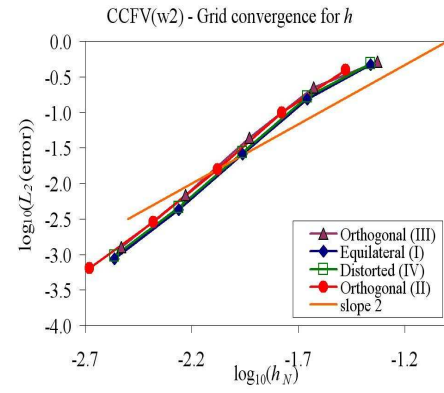
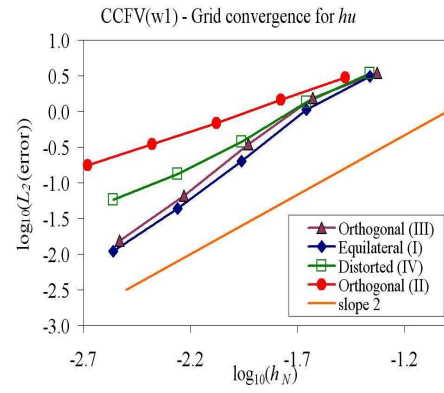
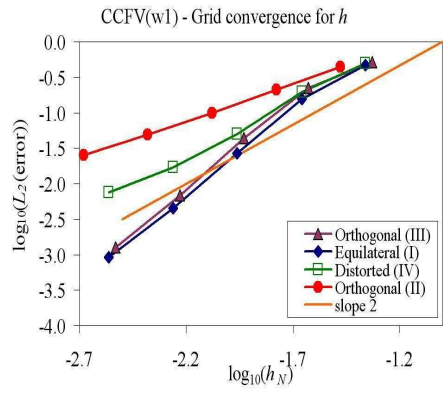
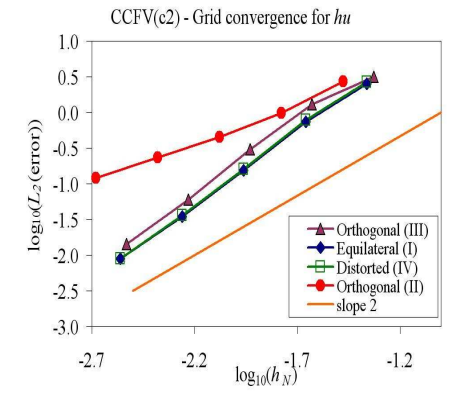
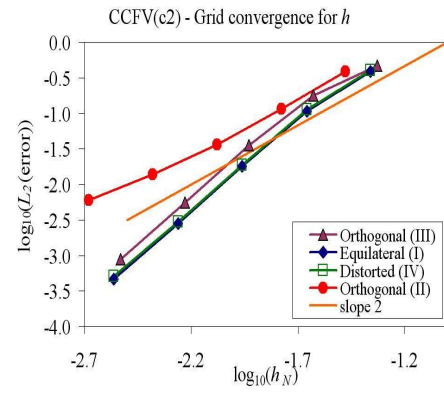
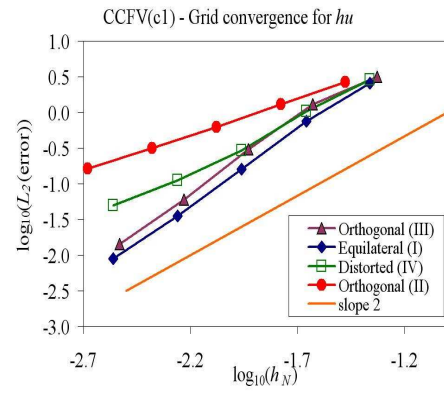
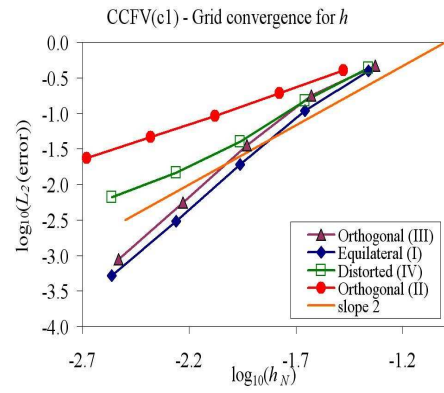


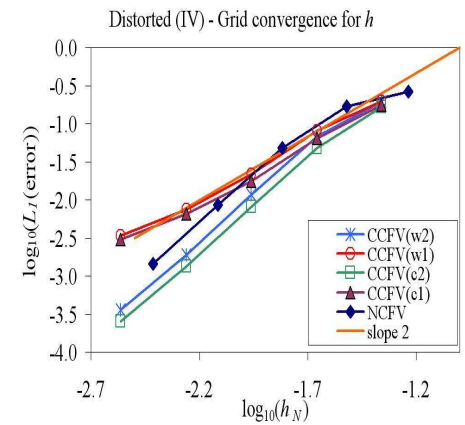
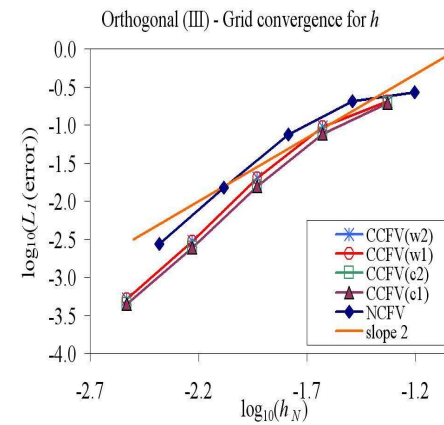
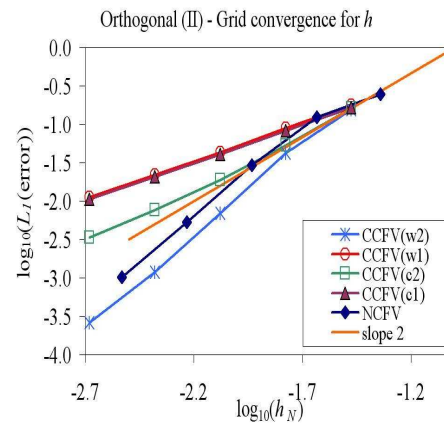
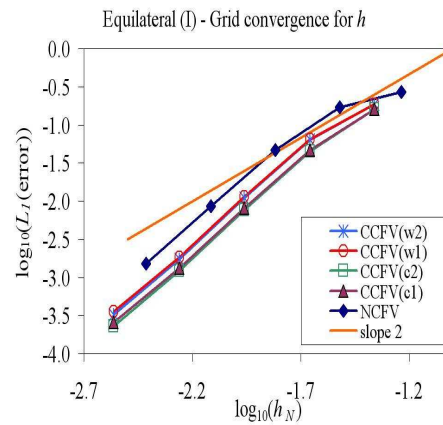
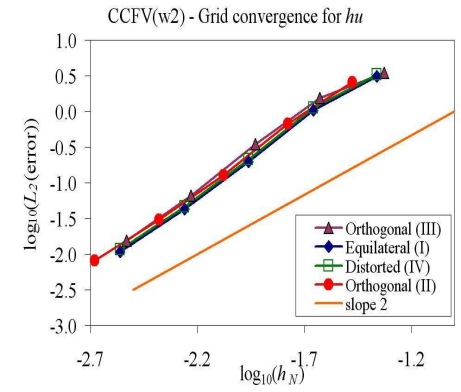
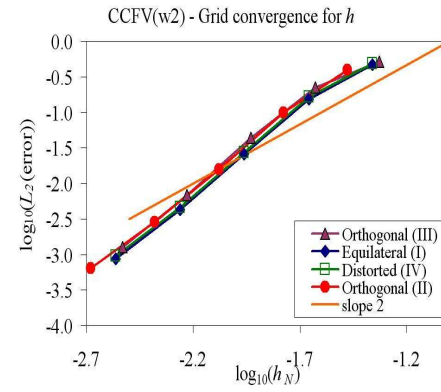
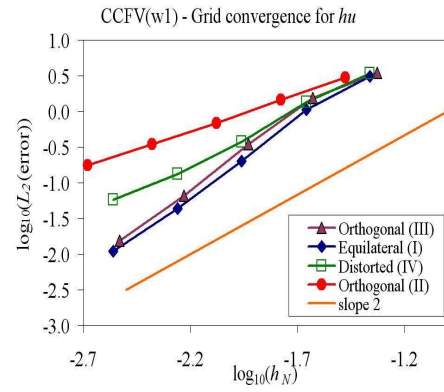
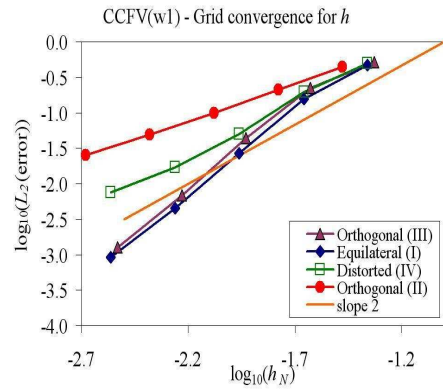
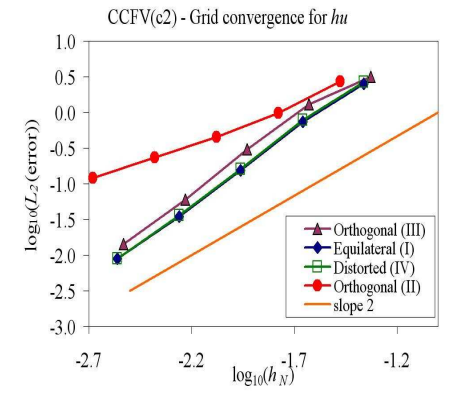
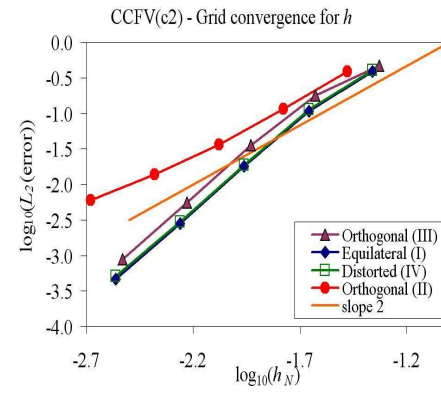
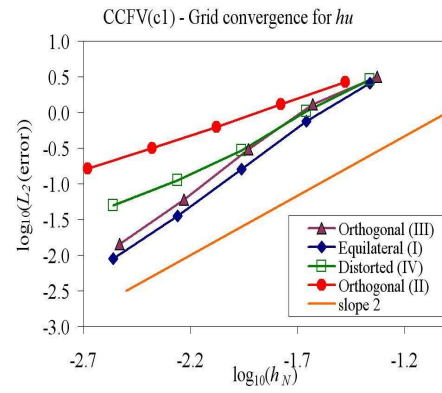
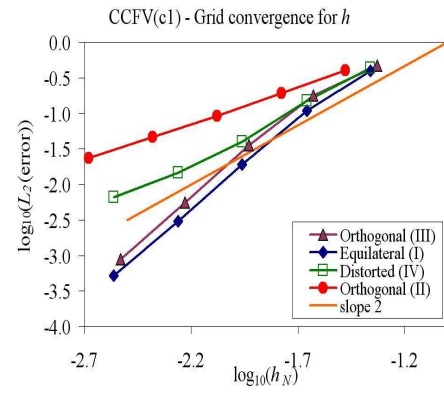




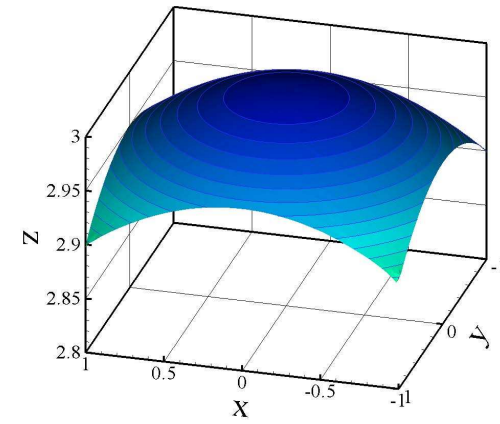
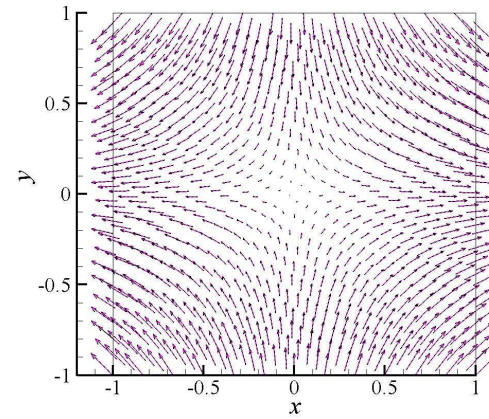
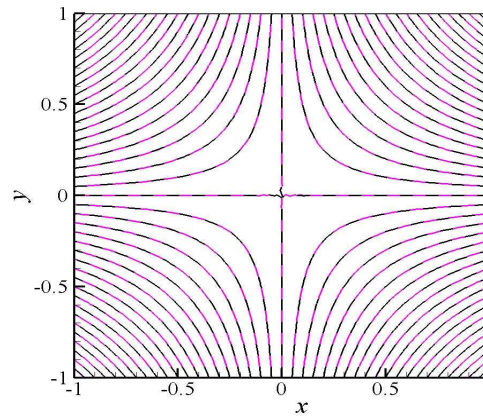
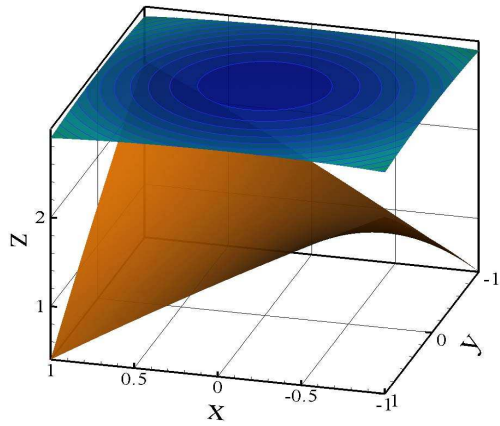




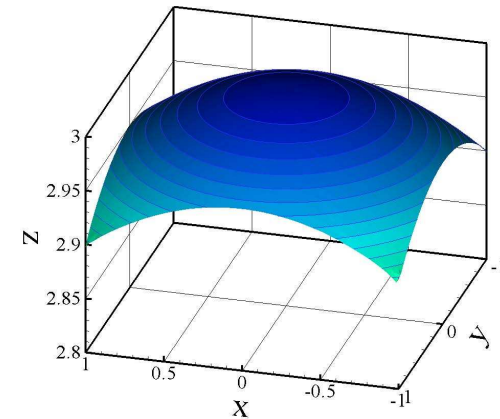
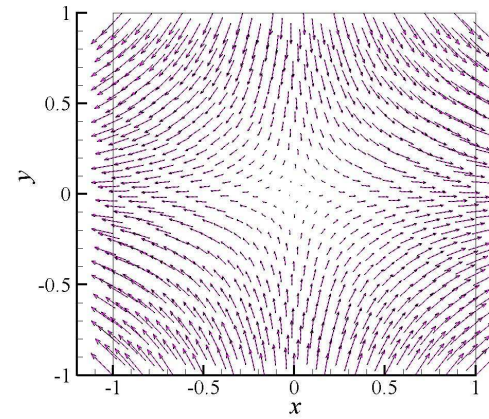
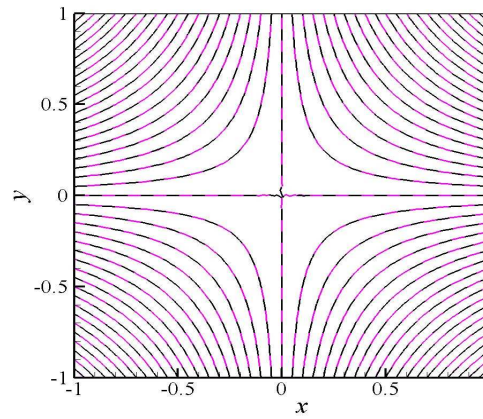
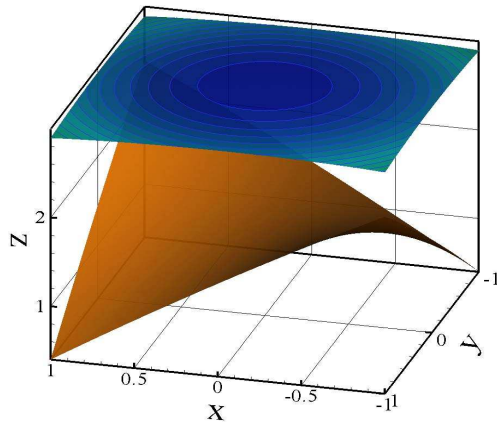




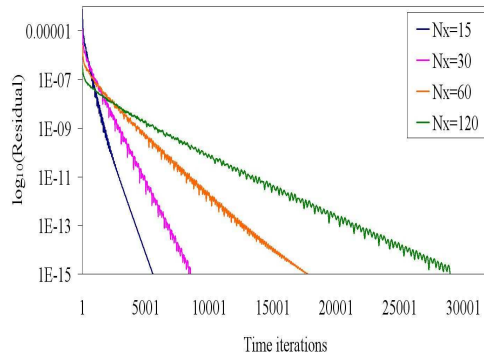
A 2D potential (steady) solution with topography



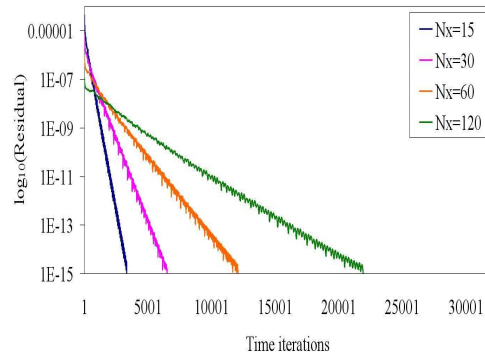
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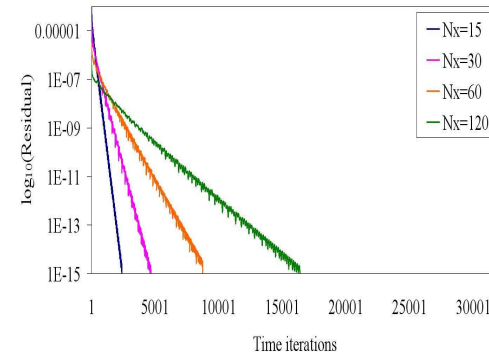
NCFV - Equilateral (I)



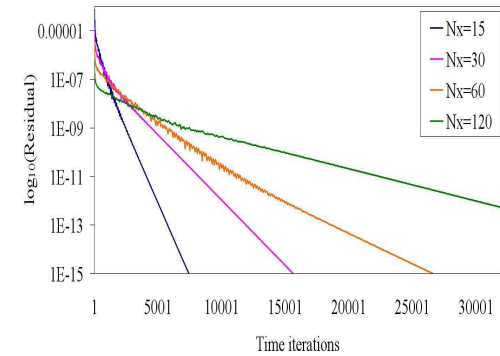
NCFV - Orthogonal (II)



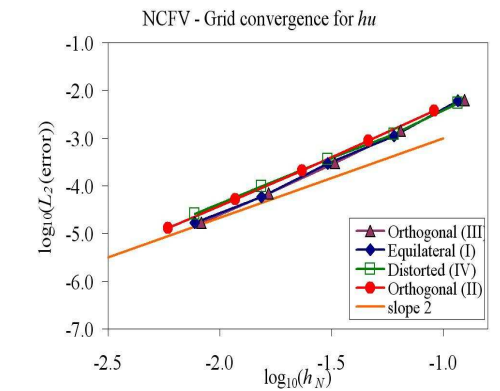
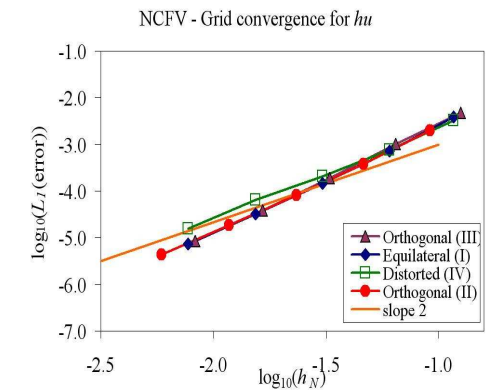
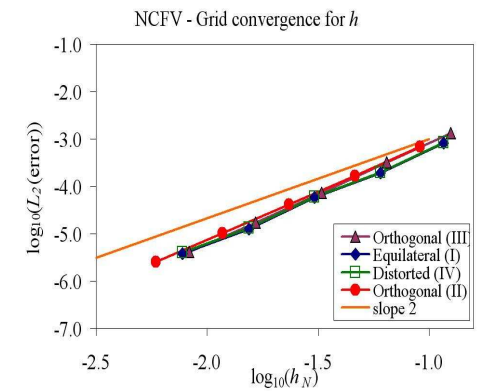
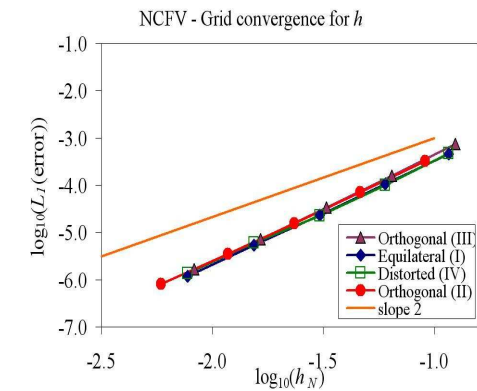
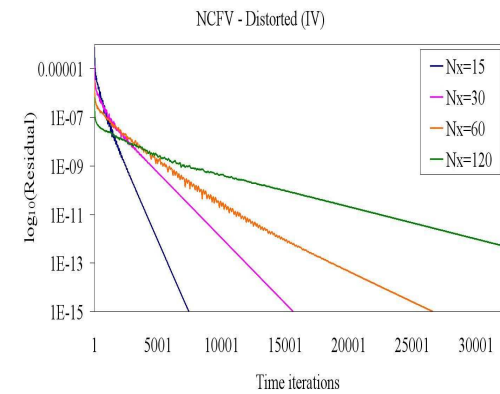
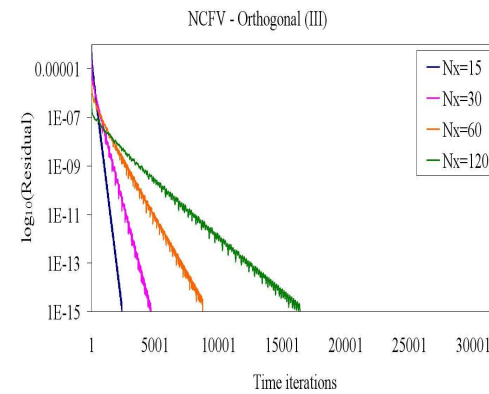
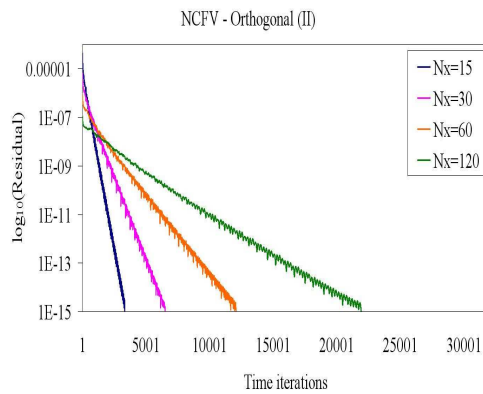
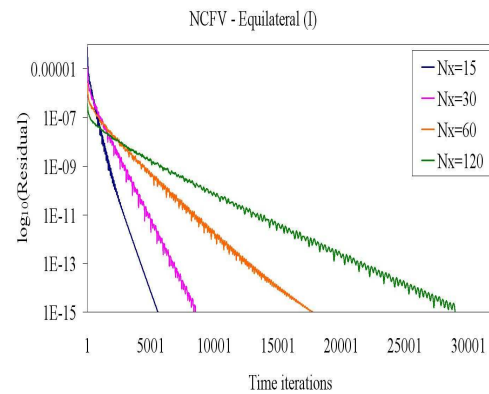
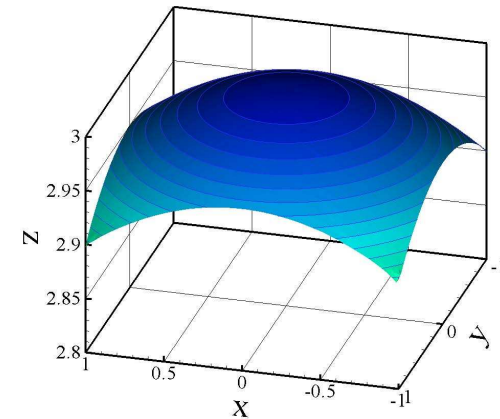
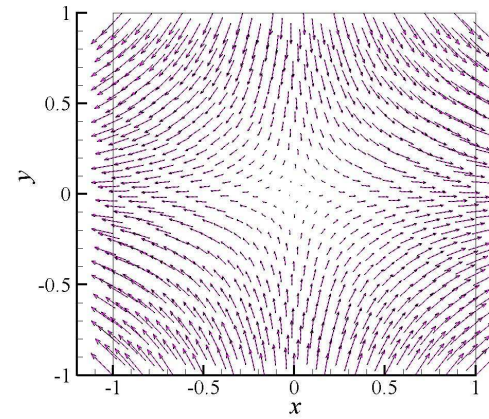
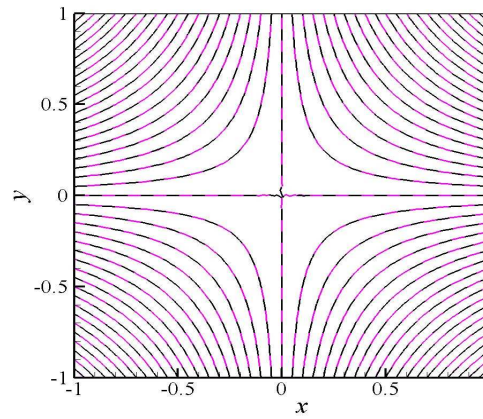
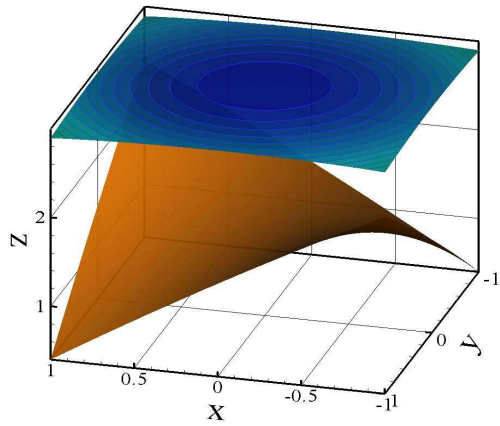
NCFV - Orthogonal (III)

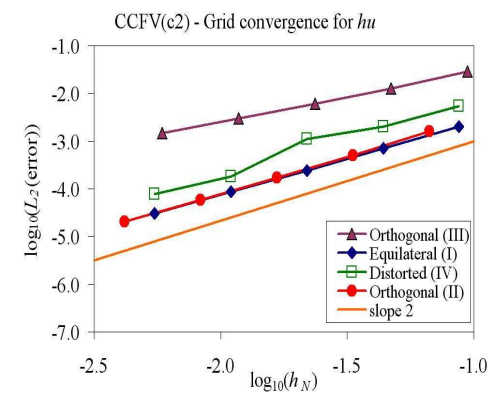
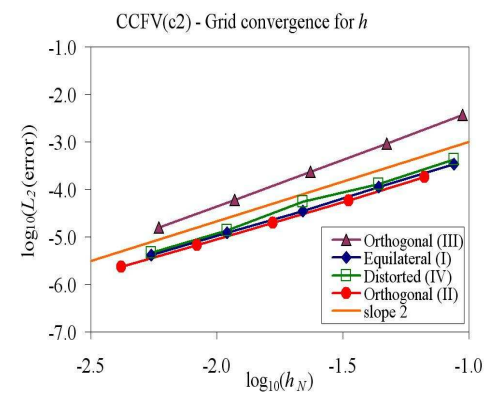
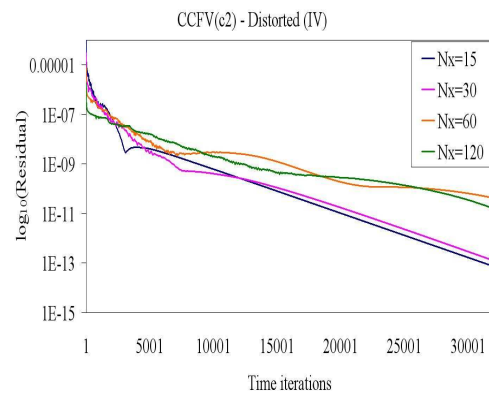
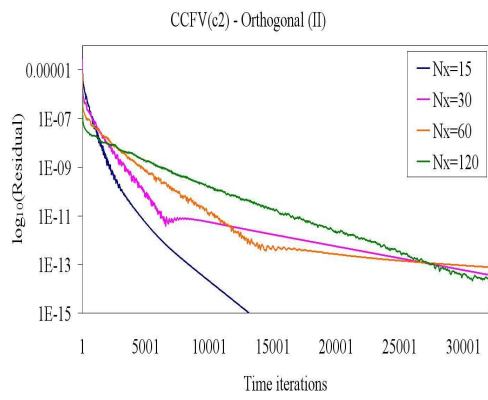


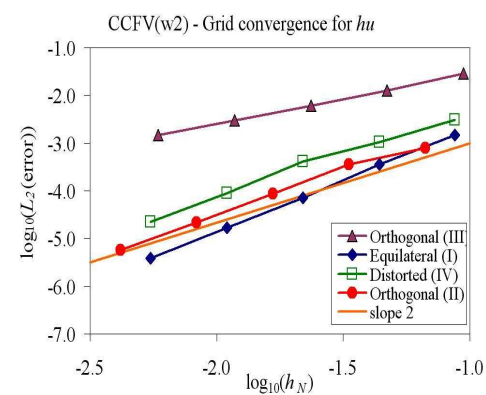
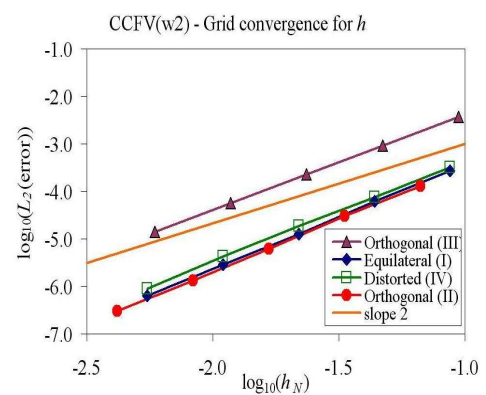
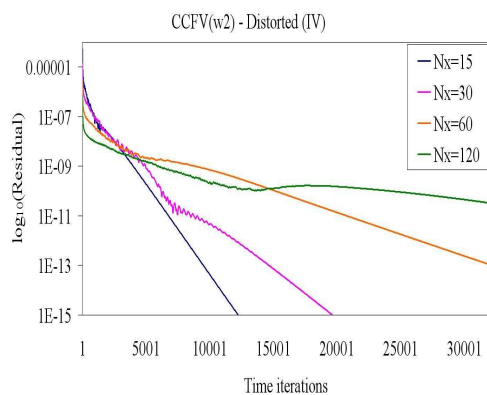
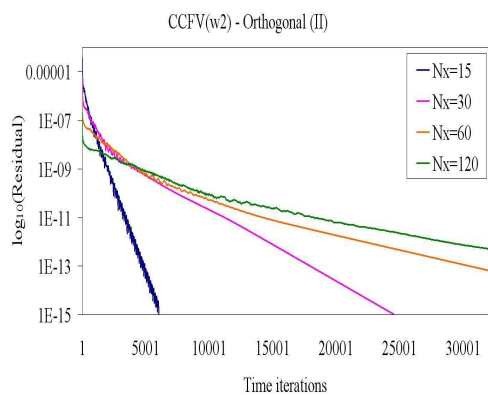
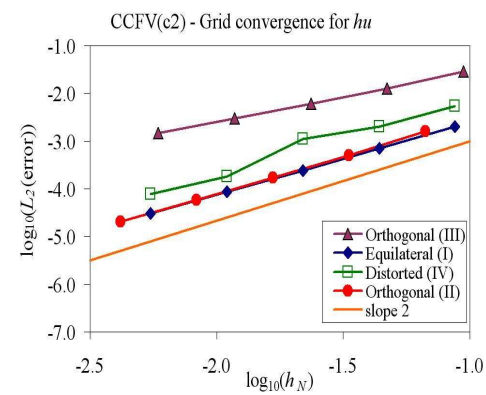
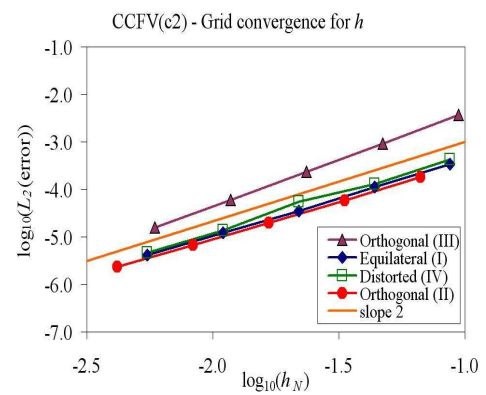
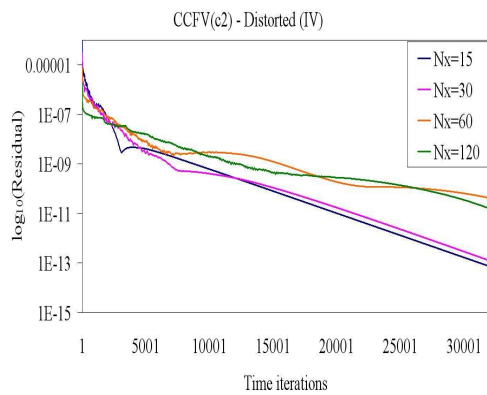
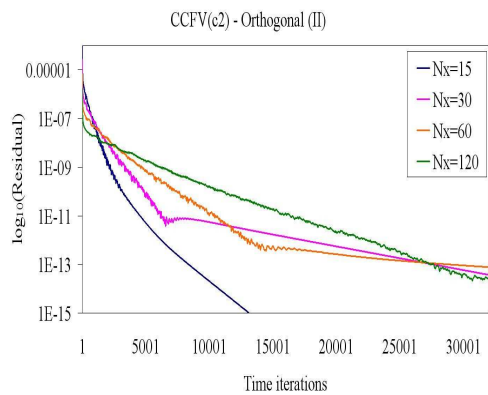
NCFV - Distorted (IV)

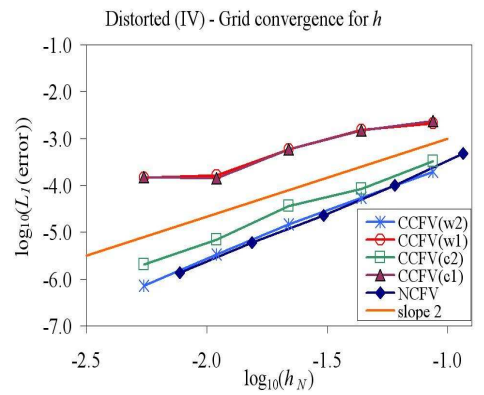
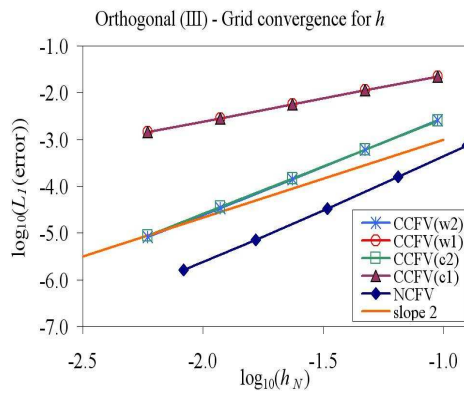
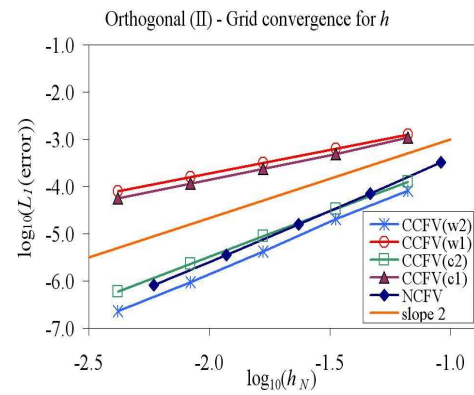
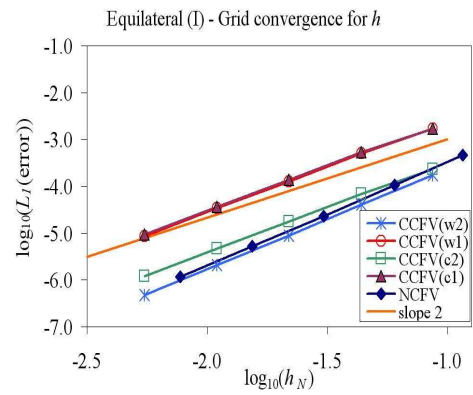
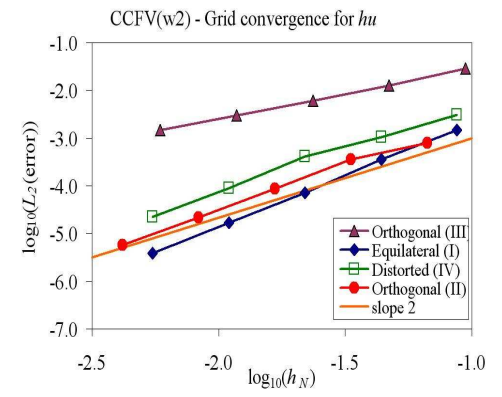
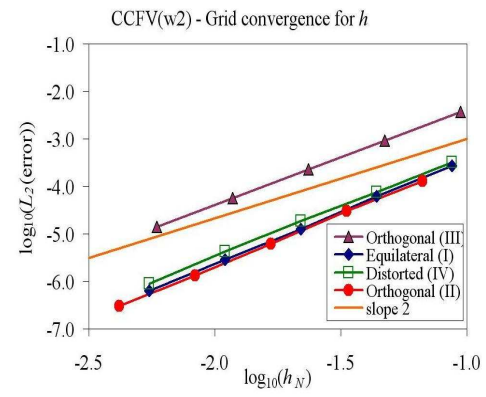
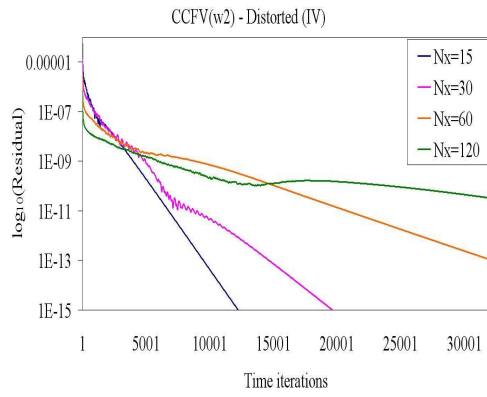
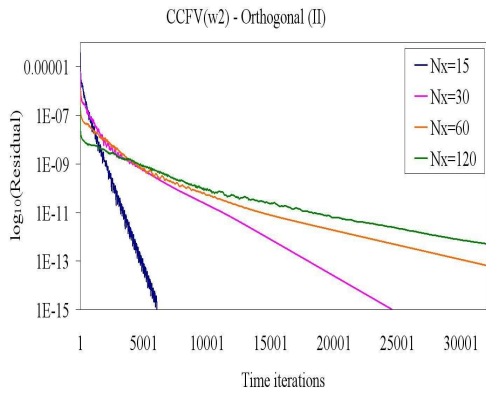
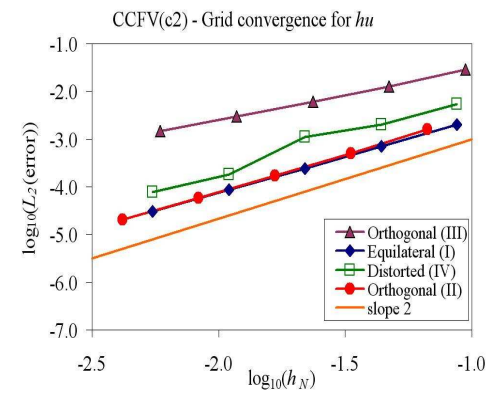
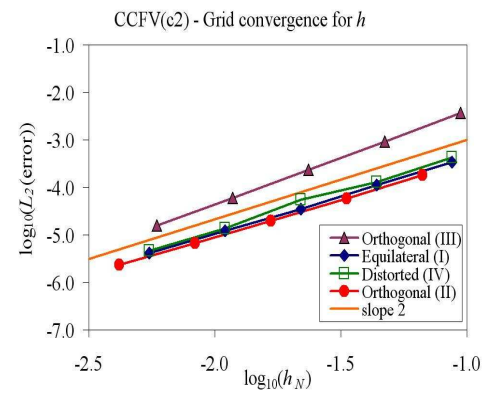
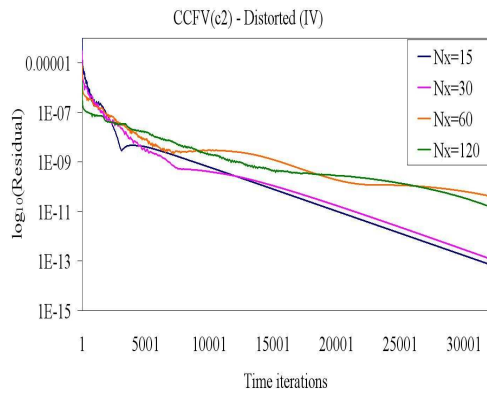
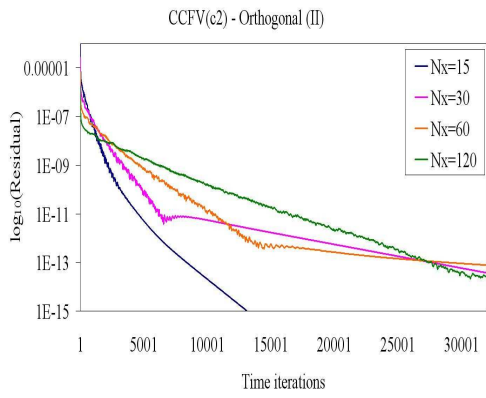


A 2D potential (steady) solution with topography



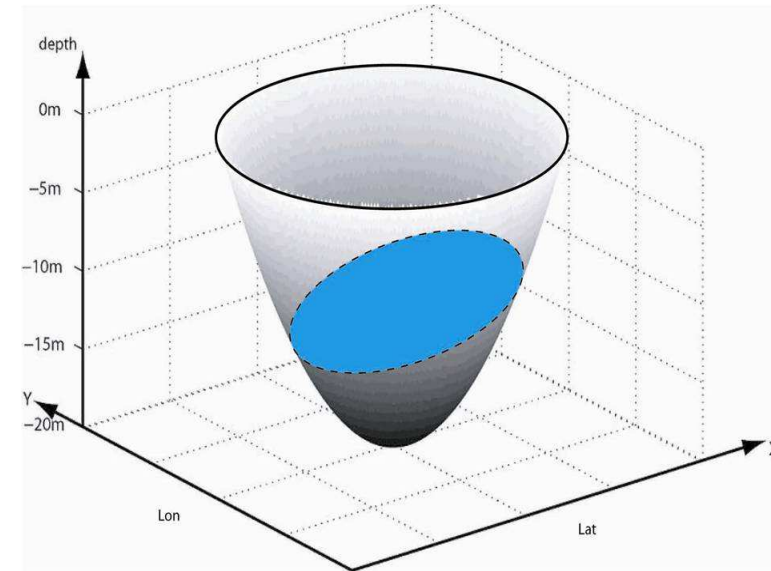






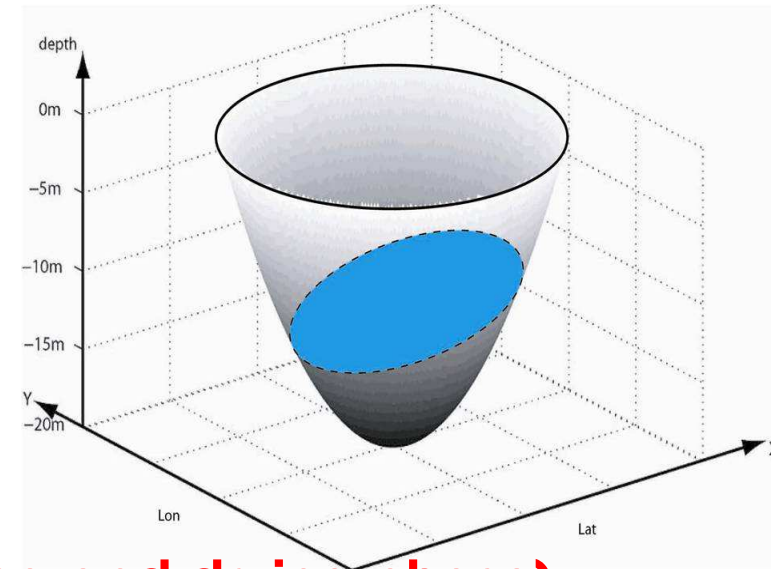
Grid convergence including dry boundaries: Thacker's 2D solutions

- Known analytical periodic solutions.
- The motion is oscillatory.
- Friction is not included.
- Difficult test (wetting and drying)
- Used it to check convergence rates.



Grid convergence including dry boundaries: Thacker's 2D solutions

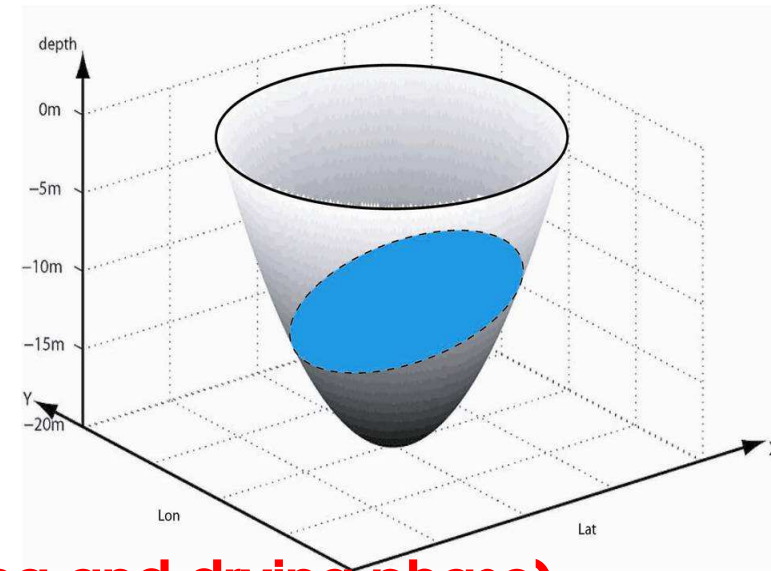
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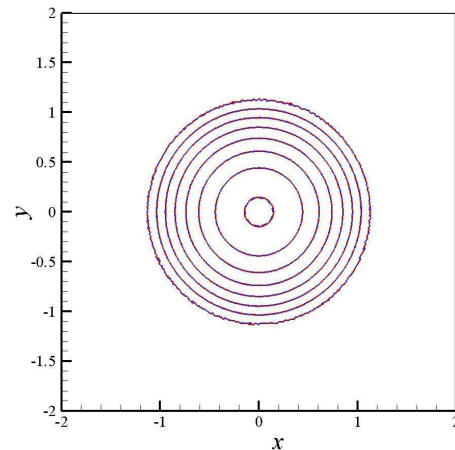
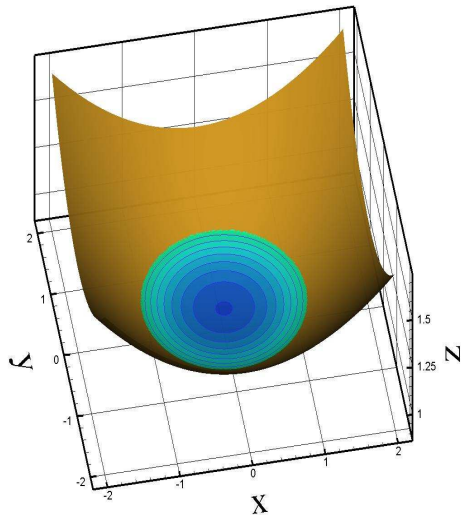
Thacker's axisymmetric solution (wetting and drying phase)

Grid convergence including dry boundaries: Thacker's 2D solutions

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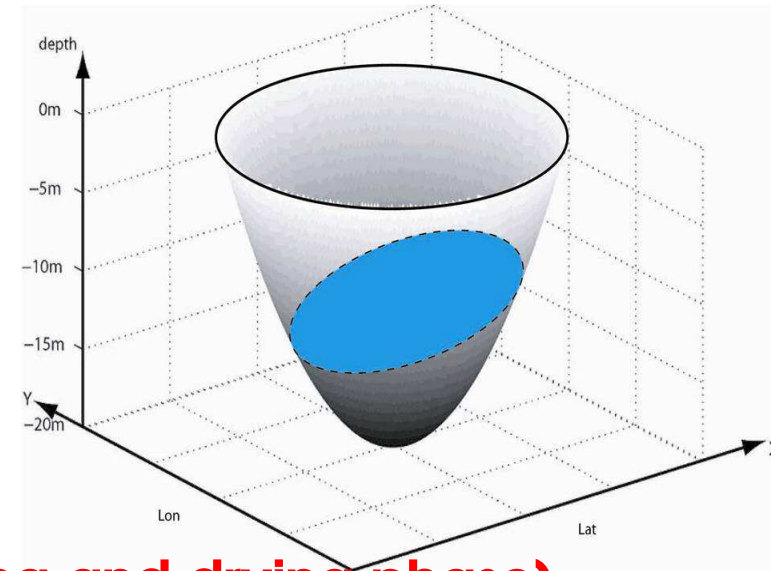


Thacker's axisymmetric solution (wetting and drying phase)

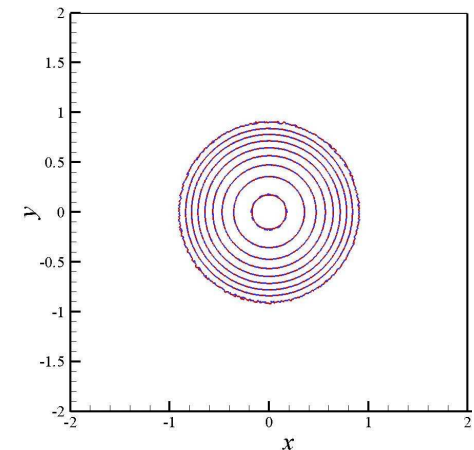
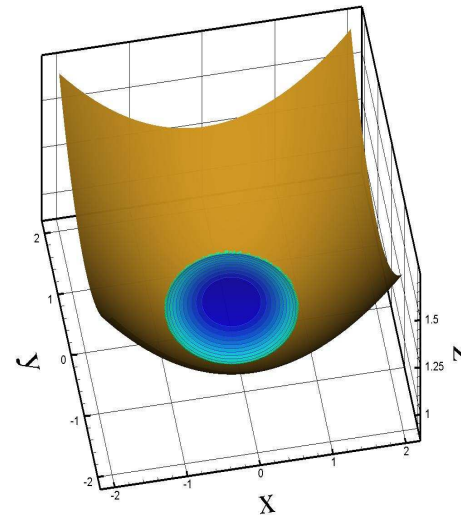
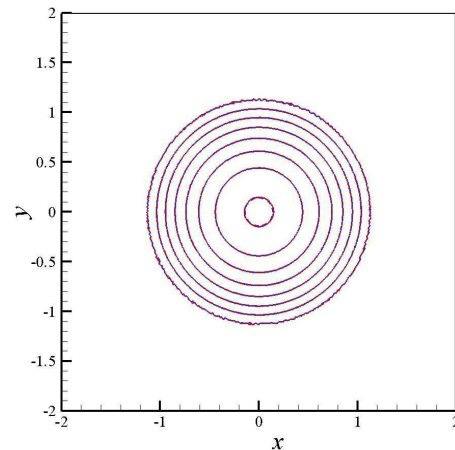
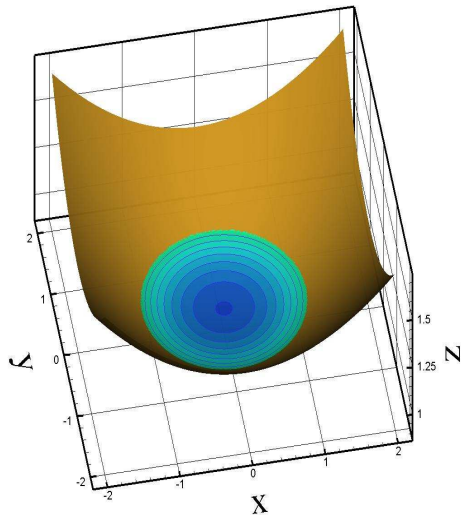


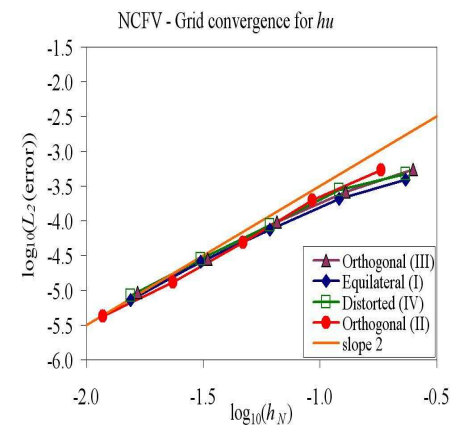
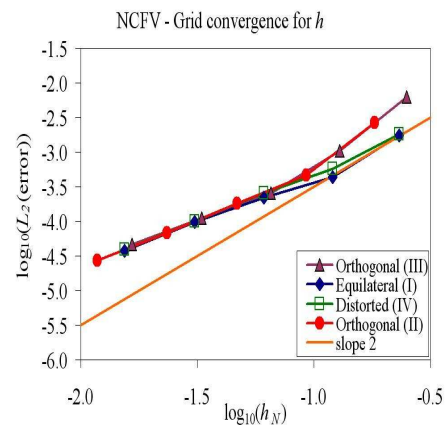
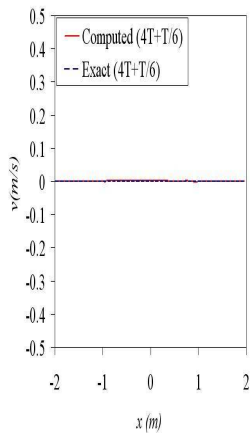
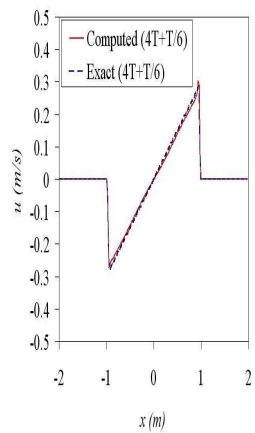
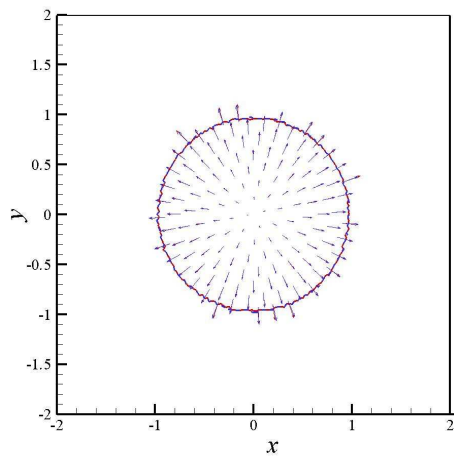
Grid convergence including dry boundaries: Thacker's 2D solutions

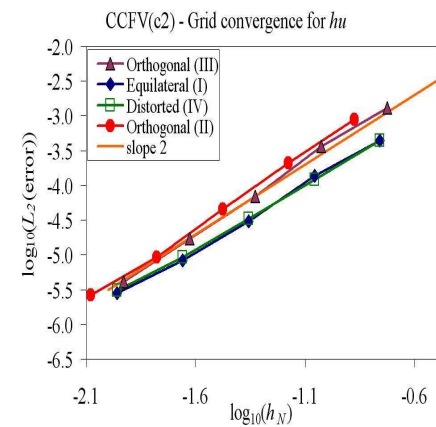
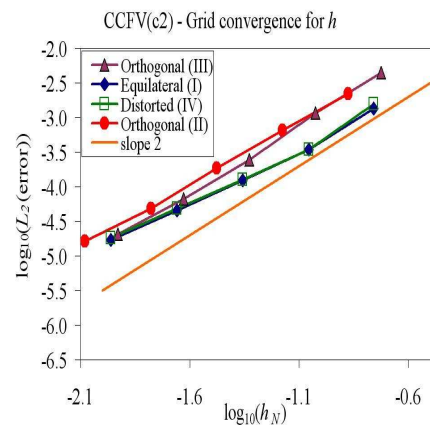
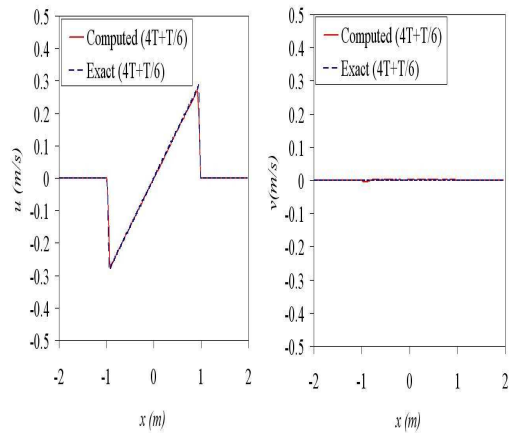
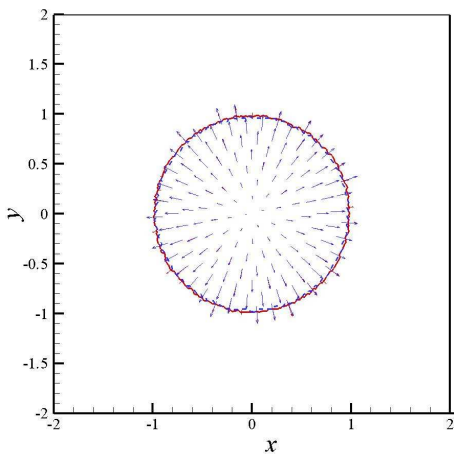
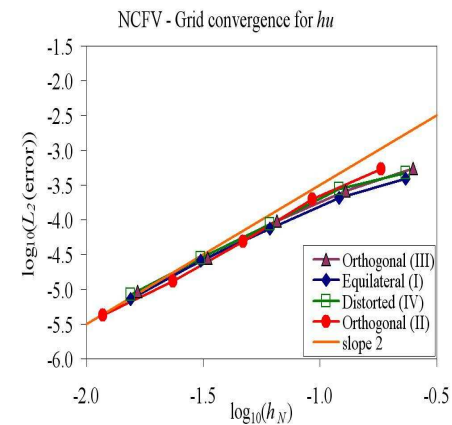
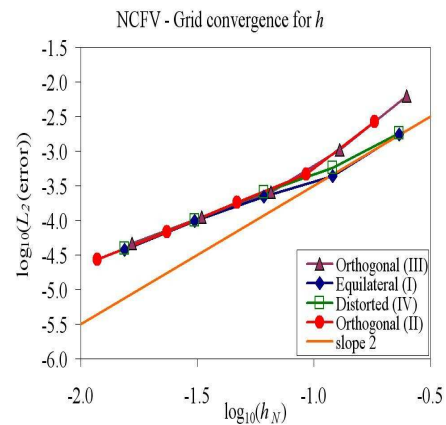
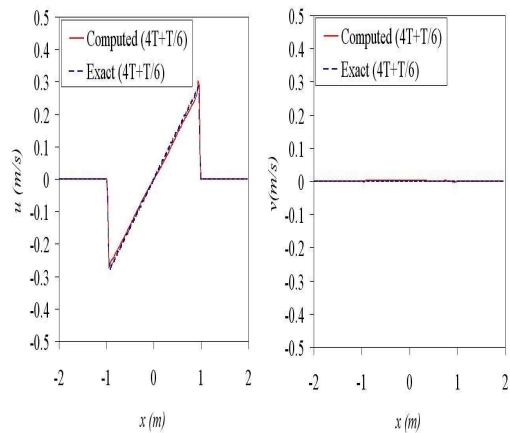
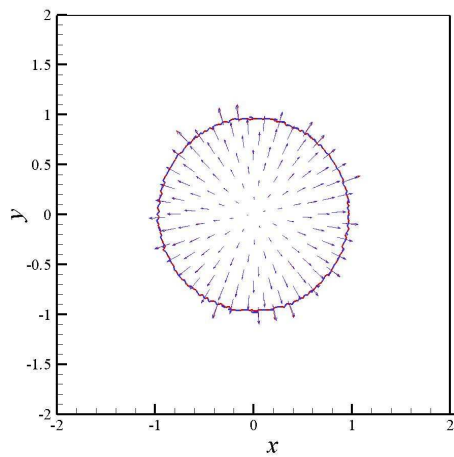
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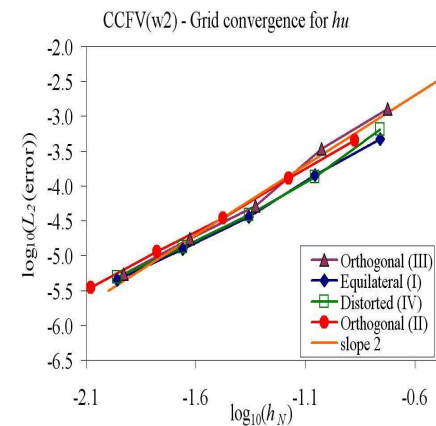
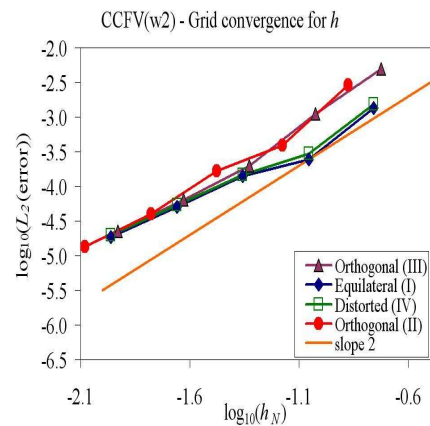
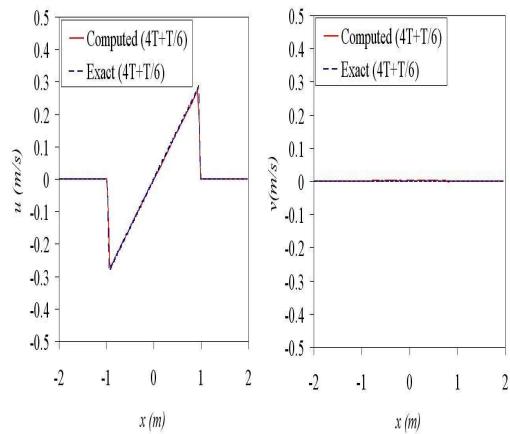
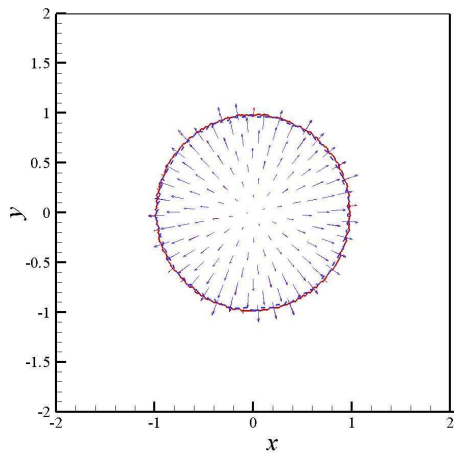
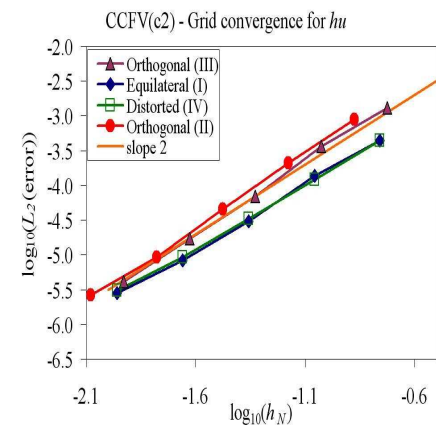
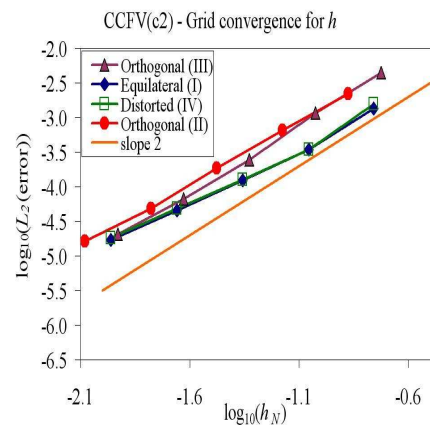
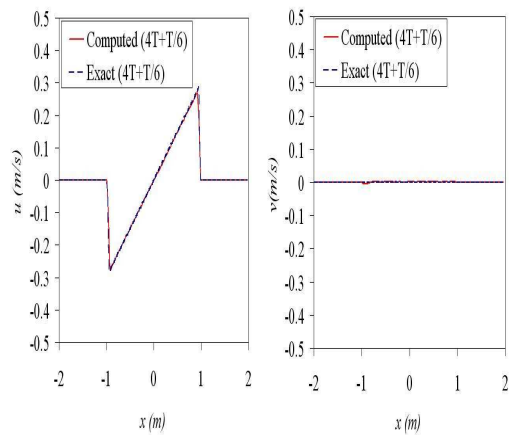
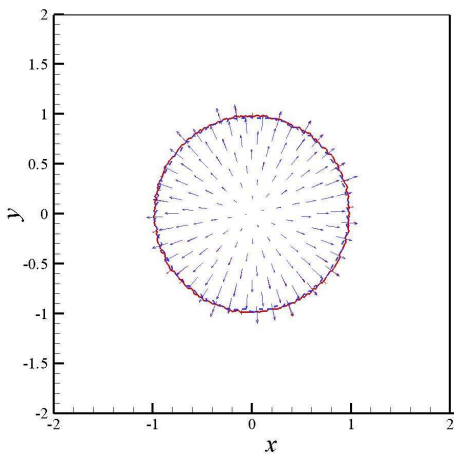
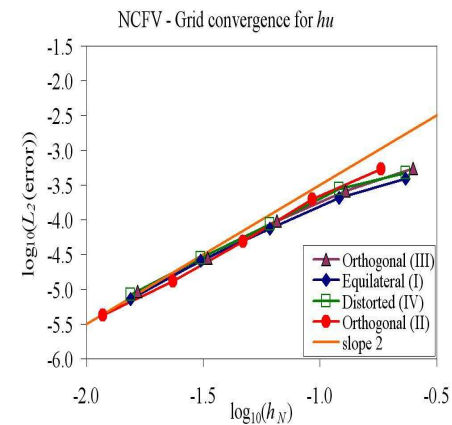
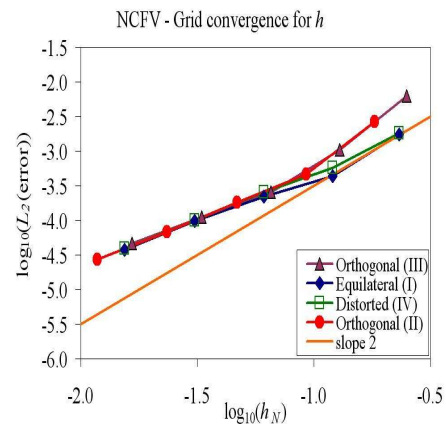
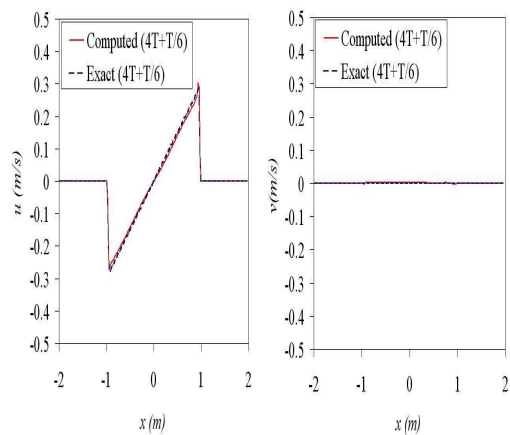
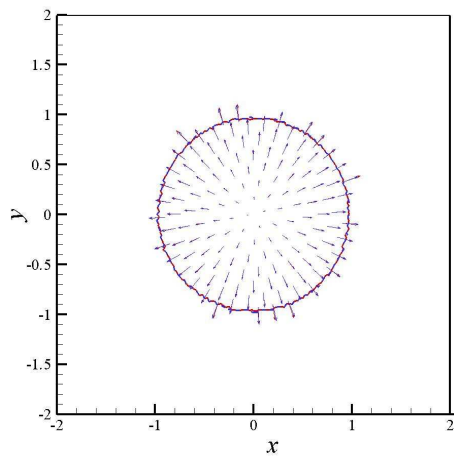


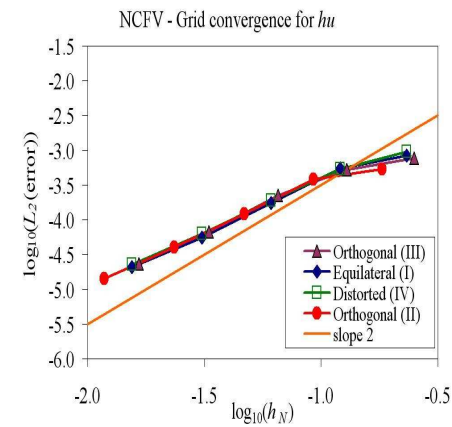
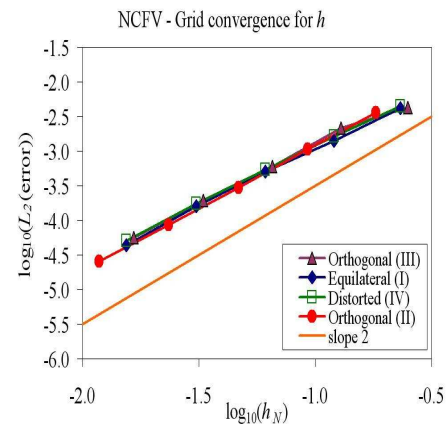
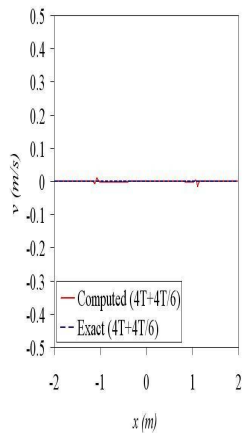
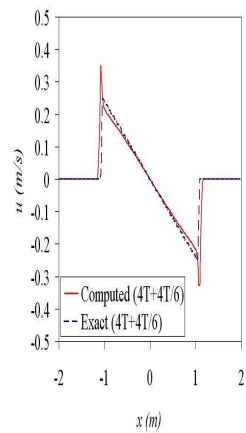
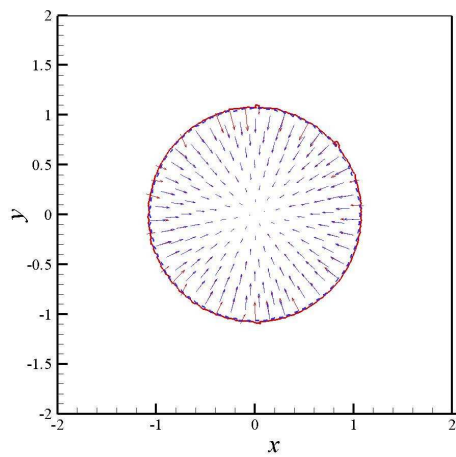
Thacker's axisymmetric solution (wetting and drying phase)

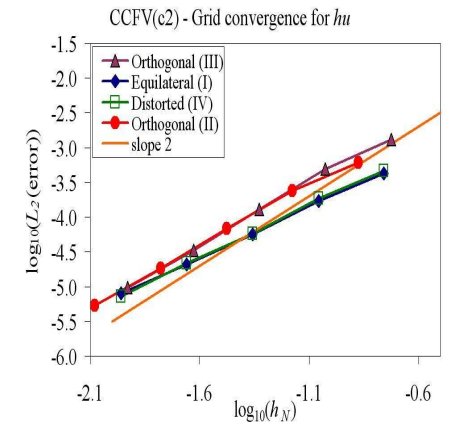
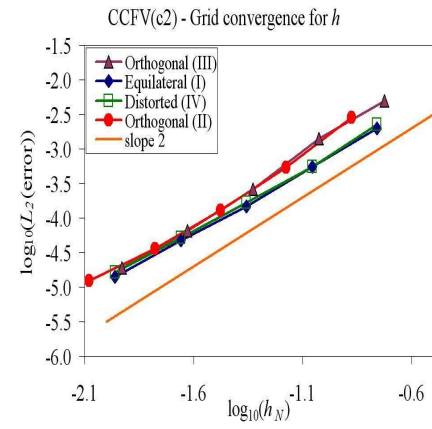
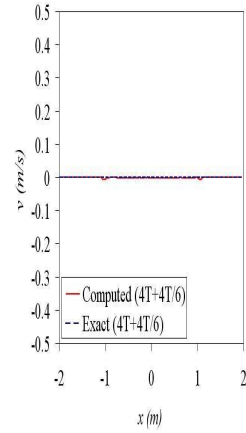
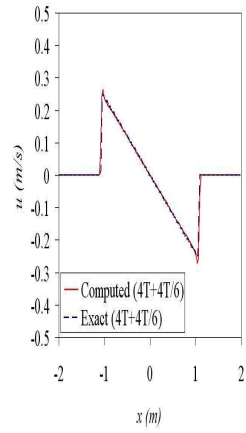
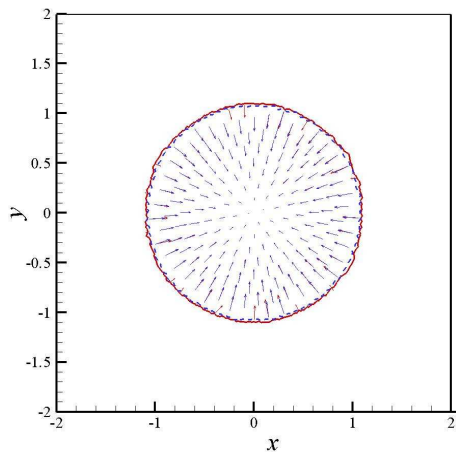
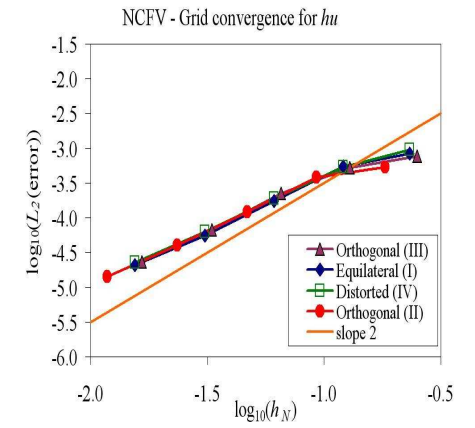
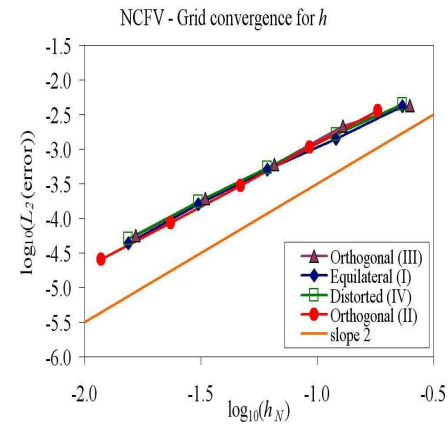
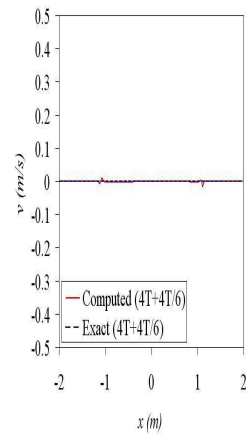
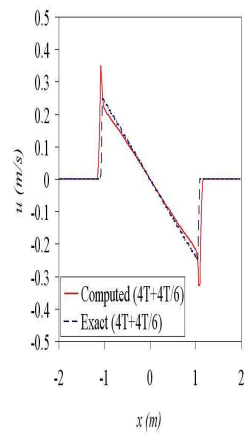
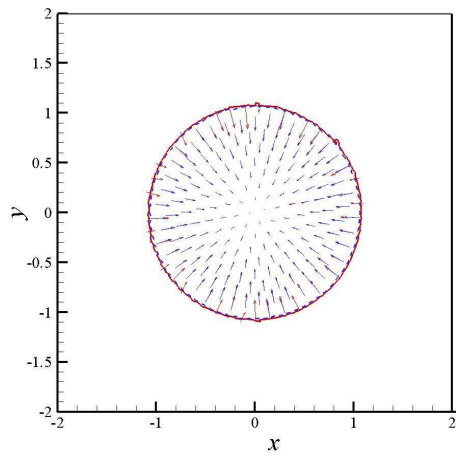


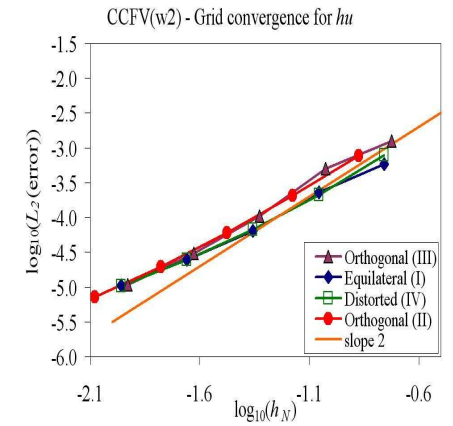
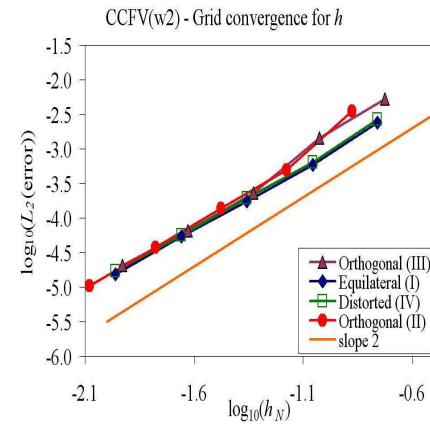
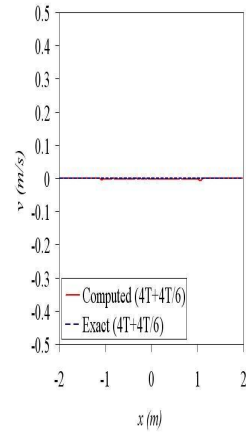
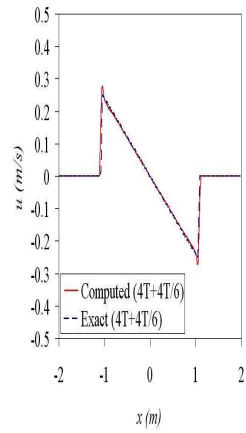
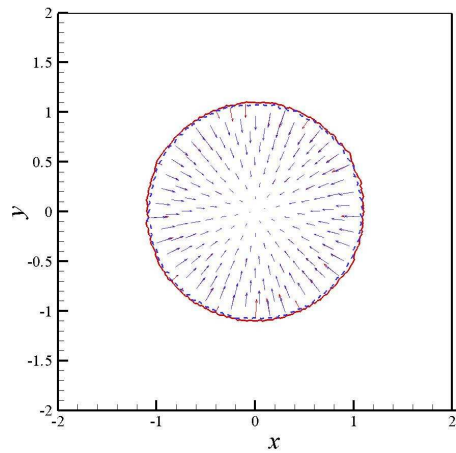
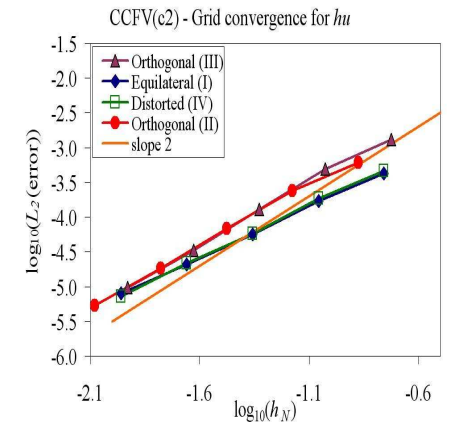
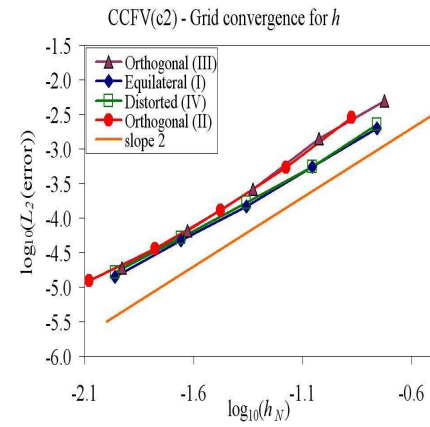
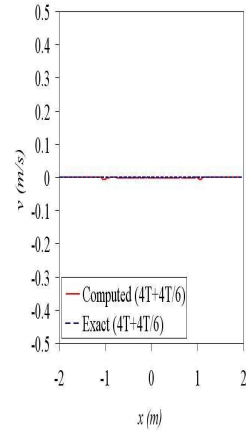
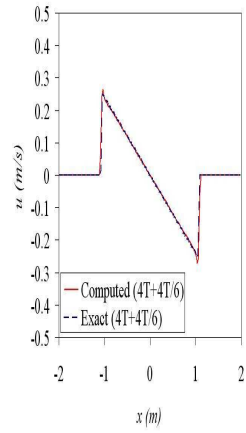
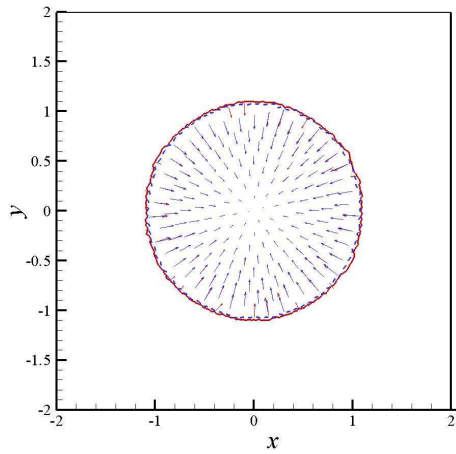
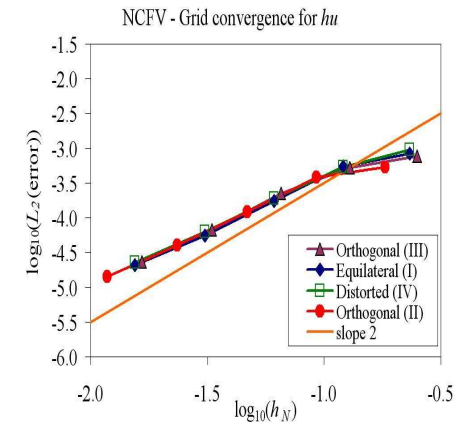
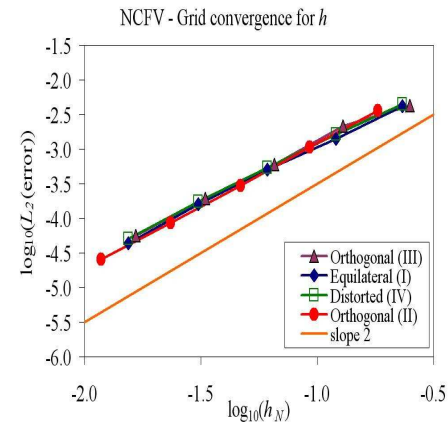
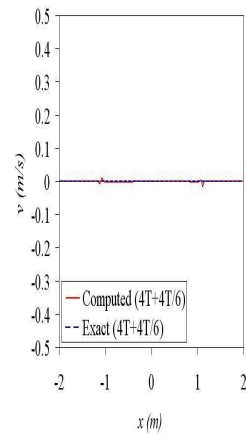
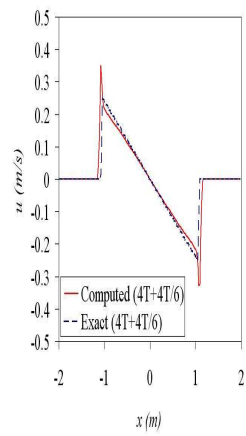
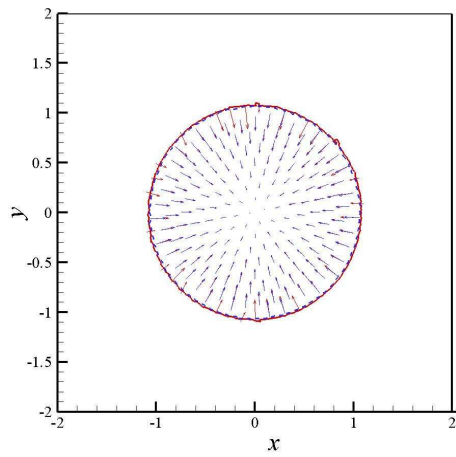








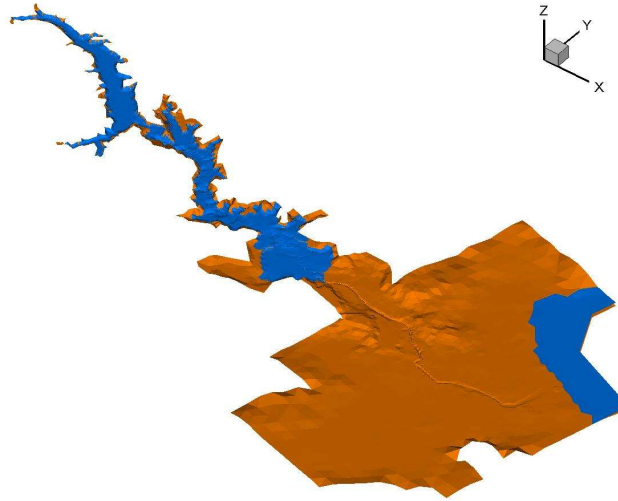




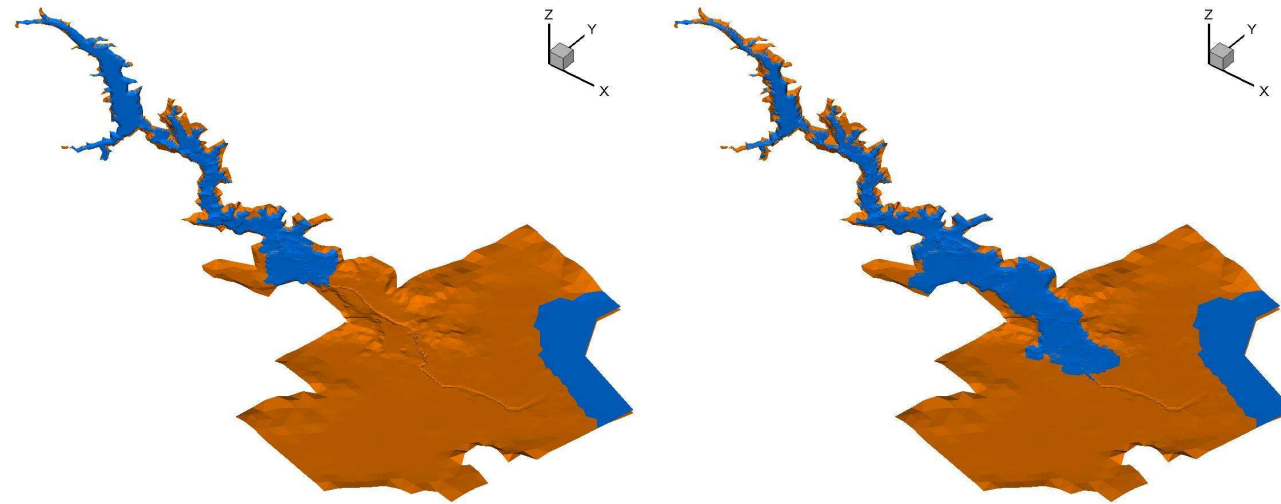
The Maplasset dam-break test case (EDF grid, CFL=0.9, $n_m = 0.033$)



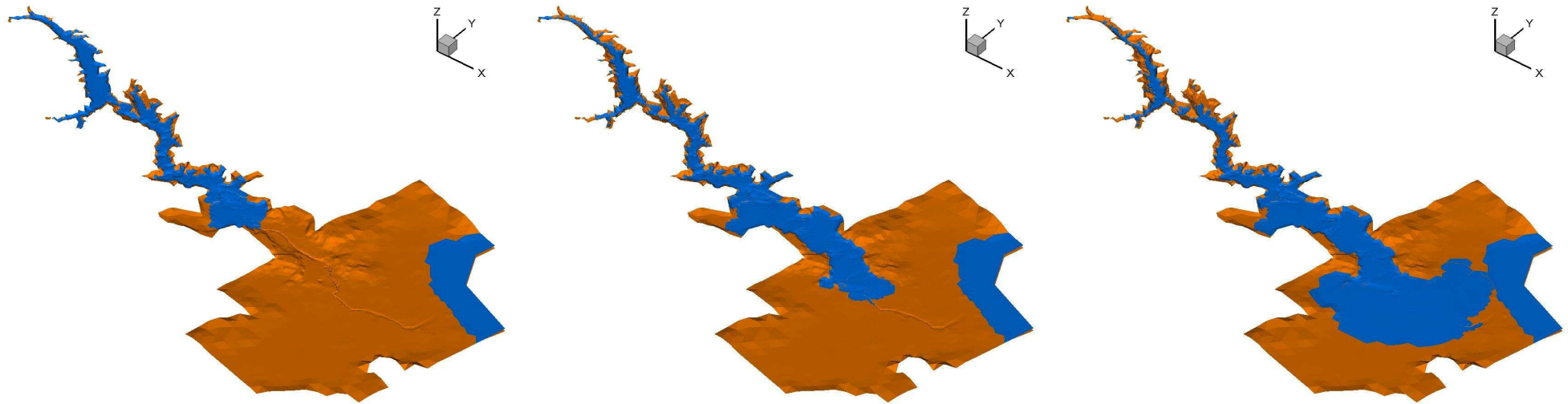
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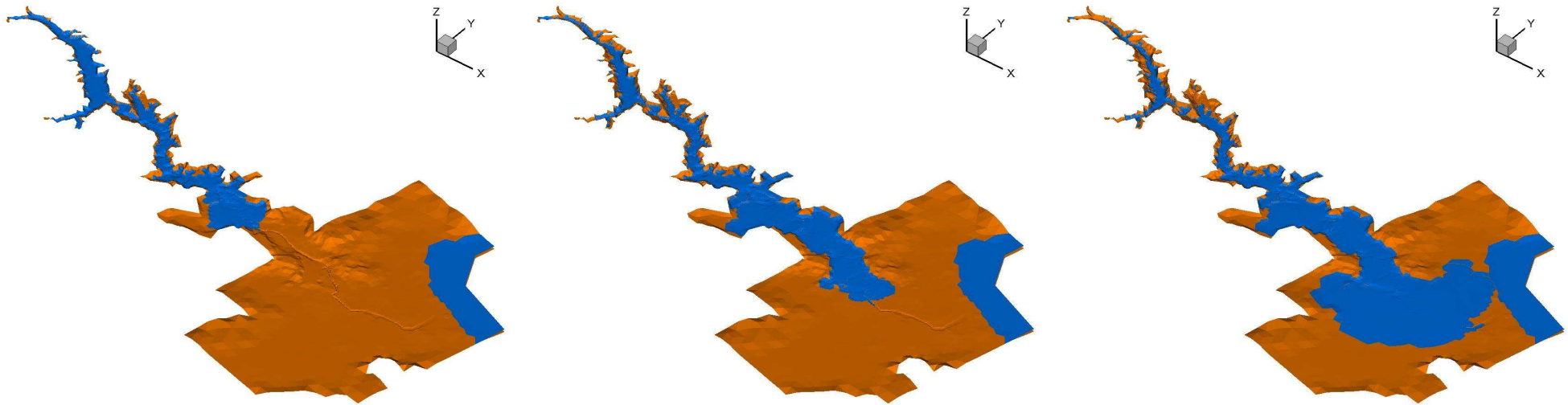


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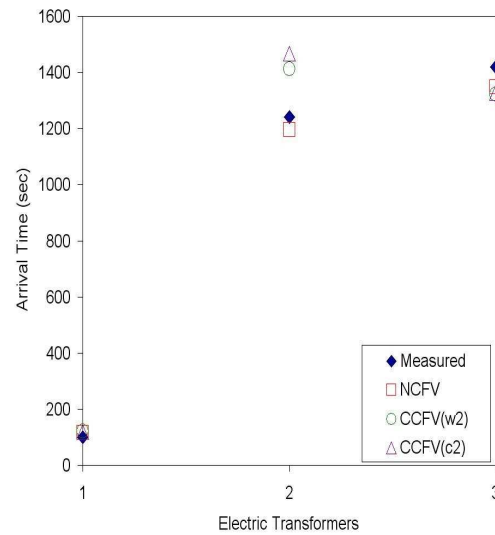


Water depth evolution at $t=800s$, $1600s$, $2400s$

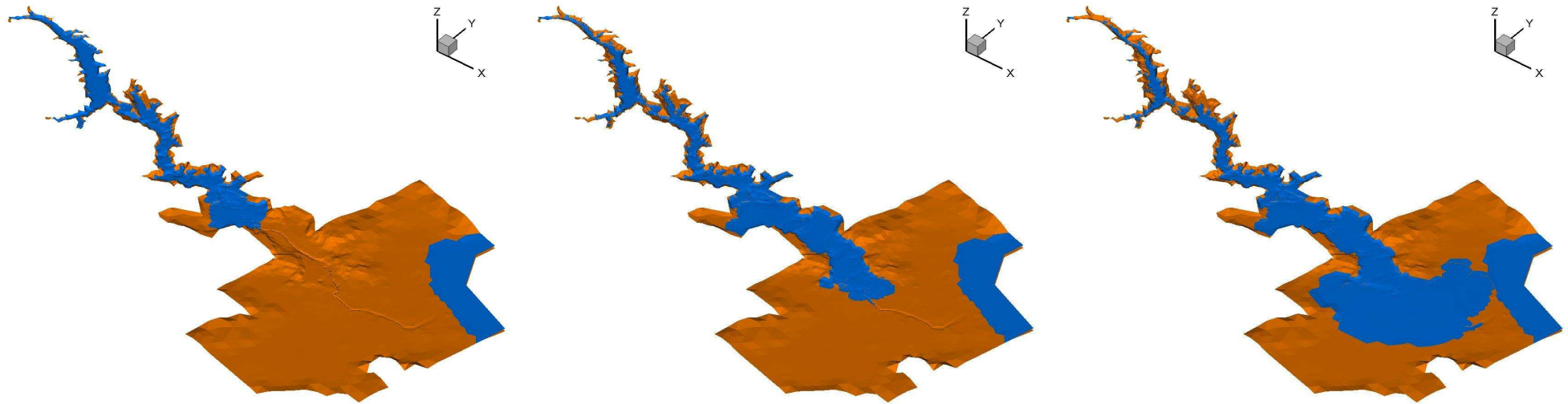
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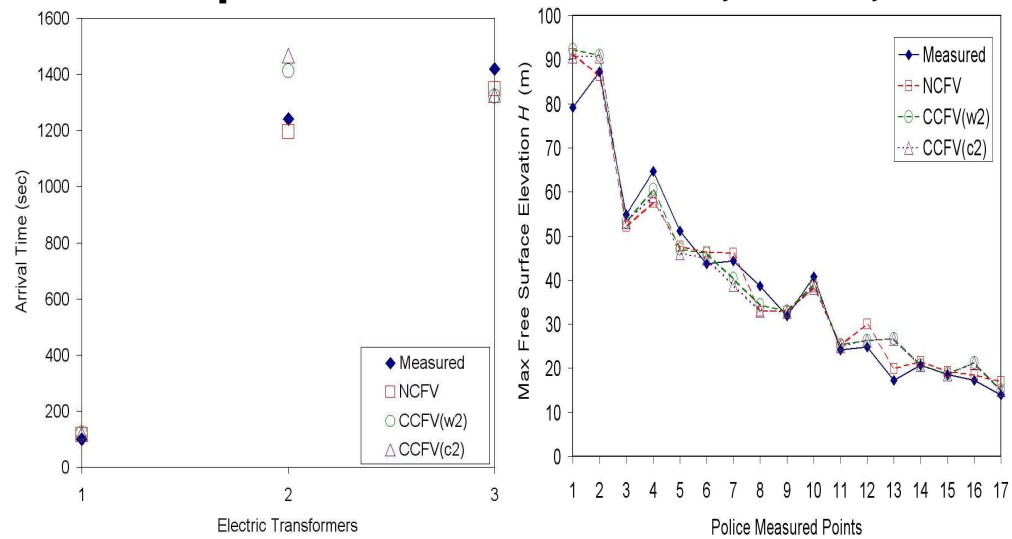
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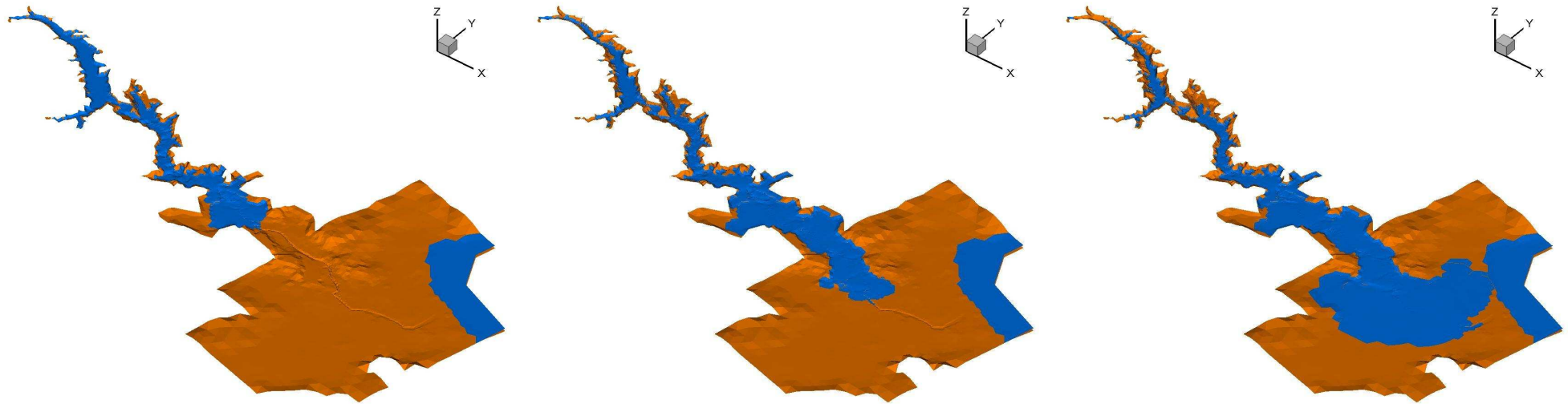
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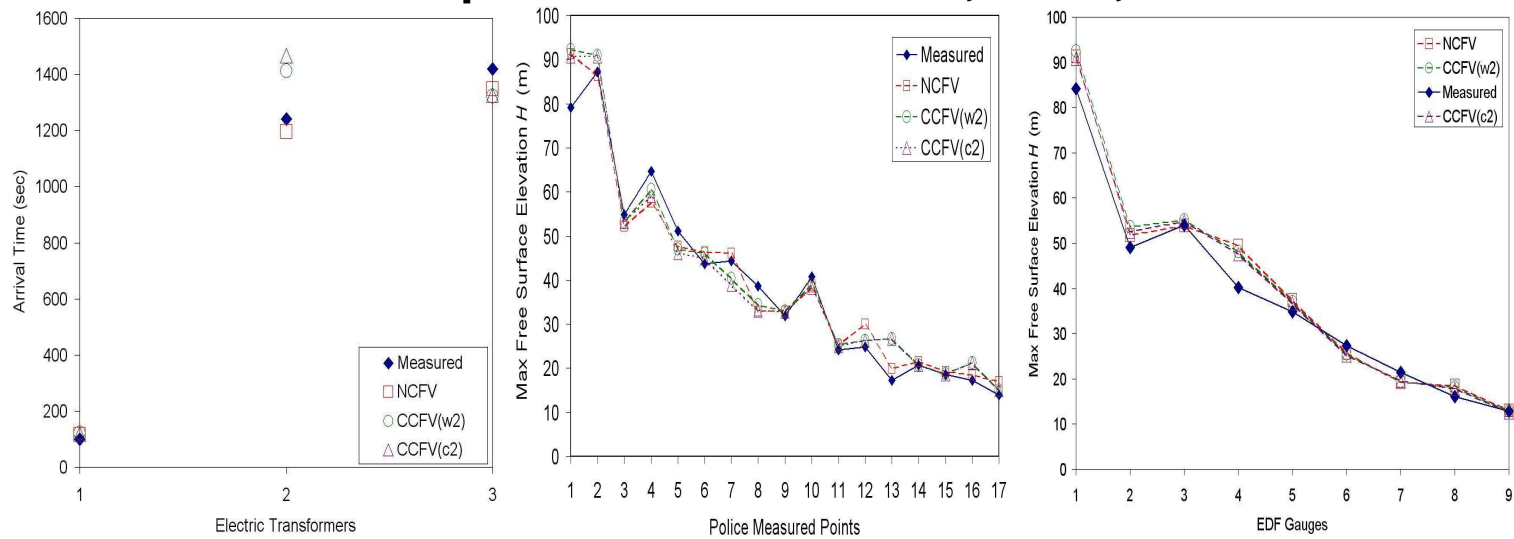
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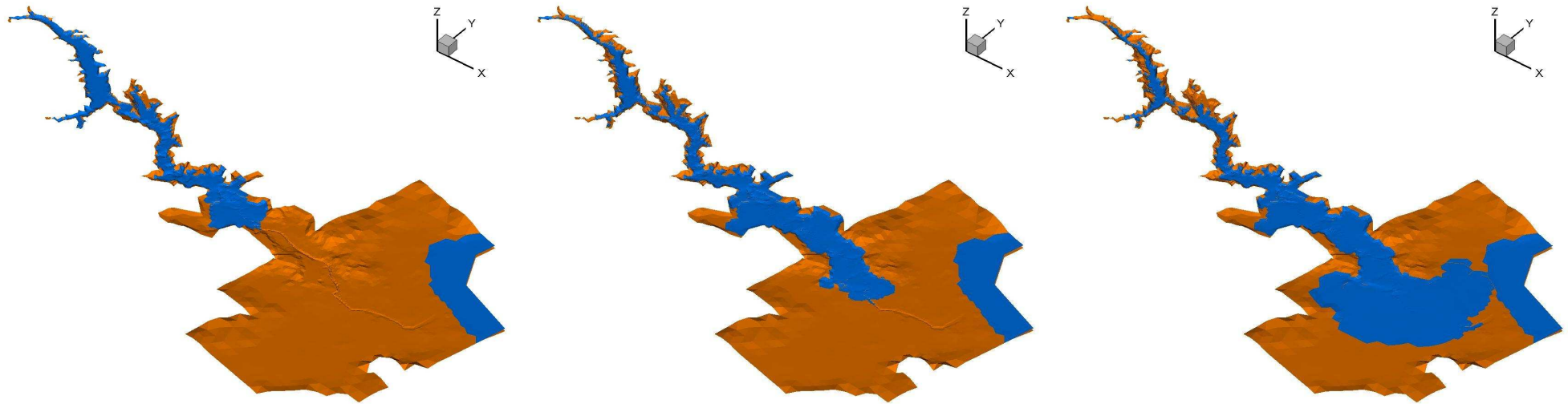
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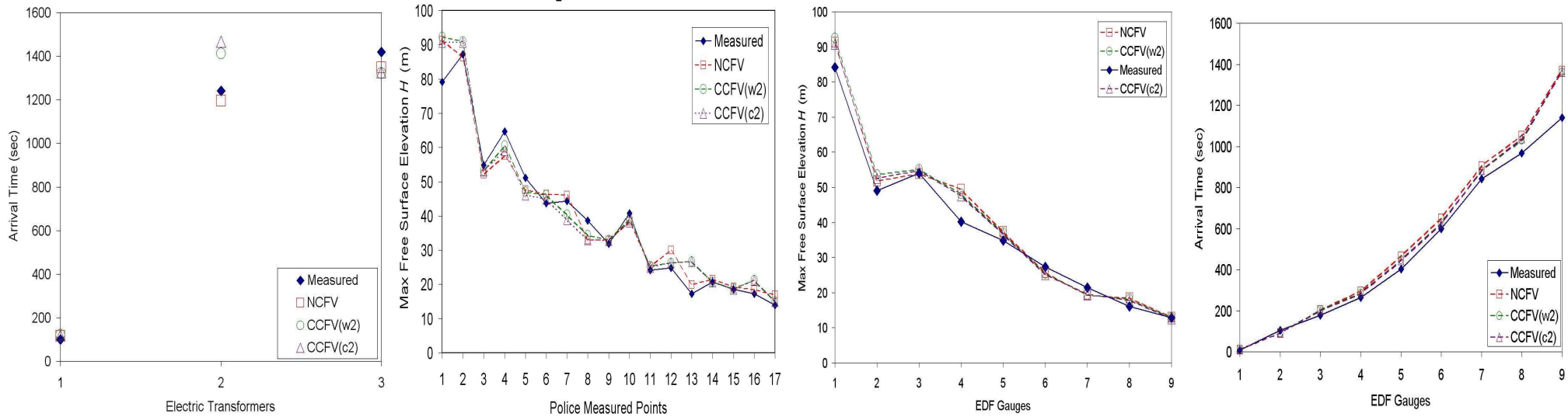
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- Both FV approaches to wetting and drying situations lead to order reduction but this drop is moderate and within acceptable limits
 - Important differences observed between the wetting and drying phase, with the results in



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References

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- I.K. Nikolos and A.I. Delis, "An unstructured nod-centered finite volume scheme for shallow water flows with wet/dry front over complex topography", Comput. Methods Appl. Mech. Engrg., 198:3723, 2009.

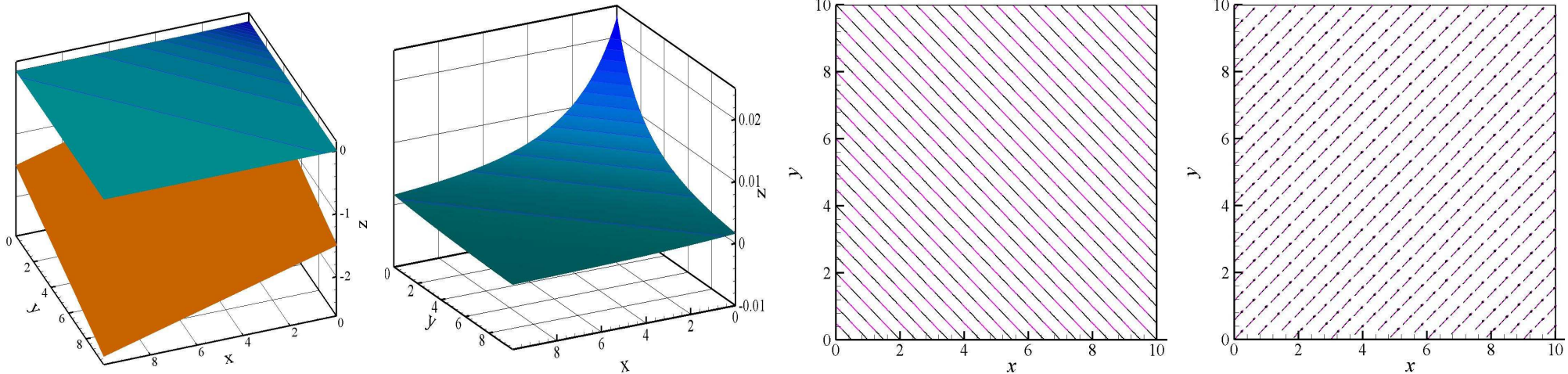
THANK YOU FOR YOUR ATTENTION!



2D steady-state with topography and friction

Known analytical solution, Murillo et al., 2007.

Start from water at rest, $n_m = 0.3$ and impose sub and super-critical boundary conditions



Compare explicit, semi-implicit and implicit friction term treatment (in terms of convergence rates)



