Unstructured Finite Volume Techniques for Boussinesq type modelling

Maria Kazolea² Argiris I. Delis¹ Costas. E. Synolakis²



¹Department of Sciences-Division of Mathematics, Technical University of Crete, Greece

² Environmental Engineering Department, TUC, Greece

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 - Gobbi, Kirby and Wei BT model (2000)
 - Variety of BT models that include higher-order nonlinear and dispersive terms: P.A. Madsen et al. (2002-2009), Lynett et al. (2004-2010) and Tissier, Bonneton et al. (2010-2012).

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- * FV for unstructured meshes: Only one work by Asmar and Nwogu (2006) using a low-order staggered scheme

Physical problem setup



- η : free surface elevation;
- *h*: **steel water level**;
- $H = \eta + h$: total water depth;
- b: bottom topography;
- *L*: wave length;
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Deep water:
$$\frac{h}{L} > \frac{1}{2}$$

Intermediate water: $\frac{1}{20} < \frac{h}{L} \leq \frac{1}{2}$

Shallow water: $\frac{h}{L} \leq \frac{1}{20}$

Mathematical Model: Nowgu's extended Boussinesq equations

Using $z_a = -0.531h$ as optimal reference depth and $u \equiv u_a$ at $z = z_a$

$$\eta_t + (Hu)_x + (Hv)_y + \left[\left(\frac{z_a^2}{2} - \frac{h^2}{6} \right) h(u_x + v_y)_x + \left(z_a + \frac{h}{2} \right) h((hu)_x + (hv)_y)_x \right]_x$$

+
$$\left[\left(\frac{z_a^2}{2} - \frac{h^2}{6}\right)h(u_x + v_y)_y + \left(z_a + \frac{h}{2}\right)h\left((hu)_x + (hv)_y\right)_y\right]_y = 0,$$
 (1)

$$u_t + g\eta_x + uu_x + vu_y + \left[\frac{z_a^2}{2}(u_{xx} + v_{yx}) + z_a\left((hu)_{xx} + (hv)_{yx}\right)\right]_t = R_{f_x} + R_{b_x}, \quad (2)$$

$$v_t + g\eta_y + uv_x + vv_y + \left[\frac{z_a^2}{2}(u_{xy} + v_{yy}) + z_a\left((hu)_{xy} + (hv)_{yy}\right)\right]_t = R_{f_y} + R_{b_y}, \quad (3)$$

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Equations derived under the assumption that

$$\epsilon := A/h \ll 1, \qquad \mu^2 := h^2/L^2 \ll 1, \qquad S := \epsilon/\mu^2 = O(1),$$

and provide good linear accuracy to $kh = \frac{2\pi h}{L} \approx 3$ (intermediate water).

Vector conservative form

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 $\mathbf{U}_t + \nabla \cdot \mathcal{H}(\mathbf{U}^*) = \mathbf{S}(\mathbf{U}) \quad \text{on} \quad \Omega \times [0, t] \subset \mathbb{R}^2 \times \mathbb{R}^+,$

U vector of the **new variables**, $\mathbf{U}^{\star} = [H, Hu, Hv]^{\mathrm{T}}$ and $\mathcal{H} = [\mathbf{F}, \mathbf{G}]$

$$\mathbf{U} = \begin{bmatrix} H \\ P_1 \\ P_2 \end{bmatrix}, \ \mathbf{F}(\mathbf{U}^{\star}) = \begin{bmatrix} Hu \\ Hu^2 + \frac{1}{2}gH^2 \\ Huv \end{bmatrix}, \ \mathbf{G}(\mathbf{U}^{\star}) = \begin{bmatrix} Hv \\ Huv \\ Hv^2 + \frac{1}{2}gH^2 \end{bmatrix},$$

with
$$\mathbf{P} = \begin{bmatrix} P_1 \\ P_2 \end{bmatrix} = H \begin{bmatrix} \frac{z_a^2}{2} \nabla (\nabla \cdot \mathbf{u}) + z_a \nabla (\nabla \cdot h\mathbf{u}) + \mathbf{u} \end{bmatrix}$$

and $\mathbf{S} = \mathbf{S_b} + \mathbf{S_d} + \mathbf{S_f}$

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and $\mathbf{S} = \mathbf{S_b} + \mathbf{S_d} + \mathbf{S_f}$
 $\mathbf{S_b} = \begin{bmatrix} 0 \\ -gHb_x \\ -gHb_y \end{bmatrix}$, $\mathbf{S_d} = \begin{bmatrix} -\psi_c \\ -u\psi_c + \psi_{M_x} \\ -v\psi_c + \psi_{M_y} \end{bmatrix}$, $\mathbf{S_f} = \begin{bmatrix} 0 \\ R_{f_x} + R_{b_x} \\ R_{f_y} + R_{b_y} \end{bmatrix}$

where

$$\psi_c = \nabla \cdot \left[\left(\frac{z_a^2}{2} - \frac{h^2}{6} \right) h \nabla (\nabla \cdot \mathbf{u}) + \left(z_a + \frac{h}{2} \right) h \nabla (\nabla \cdot h \mathbf{u}) \right]$$

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Vector conservative form (cont.)

$$\psi_{\mathbf{M}} = \begin{bmatrix} \psi_{M_x} \\ \psi_{M_y} \end{bmatrix} = H_t \frac{z_a^2}{2} \nabla (\nabla \cdot \mathbf{u}) + H_t z_a \nabla (\nabla \cdot h \mathbf{u})$$



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$$\mathbf{R}_f = [R_{f_x} R_{f_y}] = [-gHS_f^x - gHS_f^y]^{\mathrm{T}}$$

where

$$S_f^x = n_m^2 \frac{u||\mathbf{u}||}{H^{-4/3}}$$
 and $S_f^y = n_m^2 \frac{v||\mathbf{u}||}{H^{-4/3}}$ Friction force, n_m = Manning coef.

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 $R_b = [R_{b_x}, R_{b_y}]^{\mathrm{T}}$ = parametrization of wave breaking characteristics where

$$R_{b_x} = \nabla \cdot \tilde{\mathbf{R}}_{b_x}, \text{ where } \tilde{\mathbf{R}}_{b_x} = \begin{bmatrix} \nu(Hu)_x & \frac{\nu}{2}((Hu)_y + (Hv)_x) \end{bmatrix}^{\mathrm{T}} \text{ and}$$
$$R_{b_y} = \nabla \cdot \tilde{\mathbf{R}}_{b_y}, \text{ where } \tilde{\mathbf{R}}_{b_y} = \begin{bmatrix} \frac{\nu}{2}((Hu)_y + (Hv)_x) & \nu(Hv)_y \end{bmatrix}^{\mathrm{T}}.$$

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- Special treatment of **wet/dry fronts**:
 - * Identify dry cells: through an adaptive (grid dependant) tolerance parameter
 - * Consistent depth reconstruction: satisfy $\nabla H = -\nabla b$ to high-order on wet/dry fronts (Delis et al., 2011)
 - * Satisfy an extended *C*-property: Redefinition of the bed slope, numerical fluxes are computed assuming temporarily zero velocity at wet/dry faces (Brufau et al., 2004)

Numerical Model: Spatial discretization

Use of **node-centered median dual** approach to create control volume C_P :



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Use of **node-centered median dual** approach to create control volume C_P :

$$\iint_{C_P} \frac{\partial \mathbf{U}}{\partial t} d\Omega + \iint_{C_P} \nabla \cdot \mathcal{H} d\Omega = \iint_{C_P} \mathbf{S} d\Omega \implies \frac{\partial}{\partial t} \iint_{C_P} \mathbf{U} d\Omega + \oint_{\partial C_P} \mathcal{H} \cdot \tilde{\mathbf{n}} dl = \iint_{C_P} \mathbf{S} d\Omega$$

Introducing the flux vectors

$$\Phi_{PQ} = \int_{\partial C_{PQ}} \left(\mathbf{F} \tilde{n}_x + \mathbf{G} \tilde{n}_y \right) dl \quad \text{and} \quad \Phi_{P,\Gamma} = \int_{\partial C_P \cap \Gamma} \left(\mathbf{F} \tilde{n}_x + \mathbf{G} \tilde{n}_y \right) dl$$

Hence, FV scheme reads

$$\frac{\partial \mathbf{U}_P}{\partial t} = -\frac{1}{|C_P|} \sum_{Q \in K_P} \mathbf{\Phi}_{PQ} - \frac{1}{|C_P|} \mathbf{\Phi}_{P,\Gamma} + \frac{1}{|C_P|} \iint_{C_P} (\mathbf{S}_{\mathbf{b}} + \mathbf{S}_{\mathbf{d}} + \mathbf{S}_{\mathbf{f}}) d\Omega$$

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Gradient and divergence edge formulas: Green-Gauss linear reconstruction on Ω_P



$$|C_P| = \frac{1}{3} |\Omega_P|$$
$$\iint_{\Omega_P} \nabla w dA = \oint_{\partial \Omega_P} w \tilde{\mathbf{n}} dl \Rightarrow (\nabla w)_P = \frac{1}{|C_P|} \sum_{Q \in K_P} \frac{1}{2} \Big(w_P + w_Q \Big) \mathbf{n}_{PQ}$$

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For boundary cells:

$$(\nabla w)_P = \frac{1}{|C_P|} \Big[\sum_{Q \in K_P} \frac{1}{2} \Big(w_P + w_Q \Big) \mathbf{n}_{PQ} + w_P \Big(\mathbf{n}_{P,1} + \mathbf{n}_{P,2} \Big) \Big]$$

$$(\nabla \cdot \mathbf{u})_P = \frac{1}{|C_P|} \Big[\sum_{Q \in K_P} \frac{1}{2} (\mathbf{u}_P + \mathbf{u}_Q) \cdot \mathbf{n}_{PQ} + \mathbf{u}_P \cdot (\mathbf{n}_{P,1} + \mathbf{n}_{P,2}) \Big]$$

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Discretization of the dispersion terms (mass equation): Integral averaging

$$\begin{split} (\psi_c)_P &= \frac{1}{|C_P|} \iint_{C_P} \nabla \cdot \left[\left(\frac{z_a^2}{2} - \frac{h^2}{6} \right) h \nabla (\nabla \cdot \mathbf{u}) + \left(z_a + \frac{h}{2} \right) h \nabla (\nabla \cdot h \mathbf{u}) \right] d\Omega \\ &= \frac{1}{|C_P|} \sum_{Q \in K_P} \left\{ \int_{\partial C_{PQ}} \left[\left(\frac{z_a^2}{2} - \frac{h^2}{6} \right) h \nabla (\nabla \cdot \mathbf{u}) \right] \cdot \tilde{\mathbf{n}} dl + \int_{\partial C_{PQ}} \left[\left(z_a + \frac{h}{2} \right) h \nabla (\nabla \cdot h \mathbf{u}) \right] \cdot \tilde{\mathbf{n}} dl \right\} \end{split}$$

Discretization of the dispersion terms (mass equation): Integral averaging

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$$\int_{\partial C_{PQ}} \left(\frac{z_a^2}{2} - \frac{h^2}{6}\right) h \nabla (\nabla \cdot \mathbf{u}) \cdot \tilde{\mathbf{n}} dl \approx \left[\left(\frac{z_a^2}{2} - \frac{h^2}{6}\right) h \right]_M \left[\nabla (\nabla \cdot \mathbf{u}) \cdot \mathbf{n}_{PQ} \right]_M,$$
$$\int_{\partial C_{PQ}} \left(z_a + \frac{h}{2}\right) h \nabla (\nabla \cdot h\mathbf{u}) \cdot \tilde{\mathbf{n}} dl \approx \left[\left(z_a + \frac{h}{2}\right) h \right]_M \left[\nabla (\nabla \cdot h\mathbf{u}) \cdot \mathbf{n}_{PQ} \right]_M$$

 $K_{PQ} := \{ R \in \mathbb{N} \mid R \text{ is a vertex of } M_{PQ} \text{ and } RQ \in \partial M_{PQ} \}$



M

R

M_{PQ}

 C_P

$$(\nabla w)_M = \frac{1}{|M_{PQ}|} \sum_{\substack{R,Q \in K_{PQ} \\ R \neq Q}} \frac{1}{2} \left(w_R + w_Q \right) \mathbf{n}_{RQ}$$

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Discretization of the dispersion terms (momentum equations):

$$\frac{1}{|C_P|} \iint_{C_P} \left(-\mathbf{u}\psi_c + \psi_{\mathbf{M}} \right) d\Omega = -\frac{\mathbf{u}_P}{|C_P|} \iint_{C_P} \psi_c d\Omega + \frac{1}{|C_P|} \iint_{C_P} \psi_{\mathbf{M}} d\Omega.$$

The ψ_c is discretized as before and the second term takes the discrete form:

$$\begin{split} (\psi_{\mathbf{M}})_{P} &= \frac{1}{|C_{P}|} \iint_{C_{P}} \psi_{\mathbf{M}} d\Omega \ = \ \frac{1}{|C_{P}|} \iint_{C_{P}} H_{t} \frac{z_{a}^{2}}{2} \nabla(\nabla \cdot \mathbf{u}) + H_{t} z_{a} \nabla(\nabla \cdot h\mathbf{u}) d\Omega \\ &= \ \frac{1}{|C_{P}|} \iint_{C_{P}} H_{t} \frac{z_{a}^{2}}{2} \nabla(\nabla \cdot \mathbf{u}) d\Omega + \frac{1}{|C_{P}|} \iint_{C_{P}} H_{t} z_{a} \nabla(\nabla \cdot h\mathbf{u}) d\Omega \\ &\approx \ \left[H_{t} \frac{z_{a}^{2}}{2} \right]_{P} [\nabla(\nabla \cdot \mathbf{u})]_{P} + [H_{t} z_{a}]_{P} [\nabla(\nabla \cdot h\mathbf{u})]_{P} \,, \end{split}$$

Numerical Model (continued)

Consider the semi-discrete scheme:

$$\frac{\partial \mathbf{U}_{P}}{\partial t} = \mathcal{L}\left(\mathbf{U}\right)$$

Time Integration (match the order of truncation errors from dispersion terms): Use 3rd order explicit Strong Stability-Preserving Runge-Kutta (SSP-RK):

$$\begin{aligned} \mathbf{U}_{P}^{(1)} &= \mathbf{U}_{P}^{(n)} + \Delta t^{n} \mathcal{L} \left(\mathbf{U}^{(n)} \right); \\ \mathbf{U}_{P}^{(2)} &= \frac{3}{4} \mathbf{U}_{P}^{(n)} + \frac{1}{4} \mathbf{U}_{P}^{(1)} + \Delta t^{n} \frac{1}{4} \mathcal{L} \left(\mathbf{U}^{(1)} \right); \\ \mathbf{U}_{P}^{(n+1)} &= \frac{1}{3} \mathbf{U}_{P}^{(n)} + \frac{2}{3} \mathbf{U}_{P}^{(2)} + \Delta t^{n} \frac{2}{3} \mathcal{L} \left(\mathbf{U}^{(2)} \right); \end{aligned}$$

Time step Δt^n estimated by a CFL stability condition as $\Delta t^n = CFL \cdot \min_P \left(\frac{R_P}{\left(\sqrt{u^2 + v^2} + c\right)_P^n} \right)$
Velocity field recovery: from new solution variables $\mathbf{P} = [P_1, P_2]^T$

At each step in the RK scheme a linear system $\mathbf{MV} = \mathbf{C}$ with $\mathbf{M} \in \mathbb{R}^{2N \times 2N}$ and $\mathbf{C} = [\mathbf{P}_1 \ \mathbf{P}_2 \cdots \ \mathbf{P}_N]^{\mathrm{T}}$, has to be solved to obtain the velocities $\mathbf{V} = [\mathbf{u}_1 \ \mathbf{u}_2 \ \cdots \ \mathbf{u}_N]^{\mathrm{T}}$. Each two rows of the system read as

$$H_P^{(i)}\left[\frac{z_a^2}{2}\nabla(\nabla\cdot\mathbf{u}) + z_a\nabla(\nabla\cdot h\mathbf{u}) + \mathbf{u}\right]_P^{(i)} = \mathbf{P}_P^{(i)}, \quad i = 1, 2, n+1.$$

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- * Convergence to the solution was obtained in one or two steps with the numerical solution for the velocities at the previous time step given as initial guess.

Wave breaking models

- Two wave breaking models are implemented and tested
- 1. Eddy viscosity approach (Keneddy et al., 2000)

$$\begin{aligned} (\mathbf{R}_{\mathbf{b}})_{P} &= \frac{1}{|C_{P}|} \iint_{C_{P}} \mathbf{R}_{\mathbf{b}} d\Omega = \frac{1}{|C_{P}|} \iint_{C_{P}} \left[\begin{array}{c} \nabla \cdot \tilde{\mathbf{R}}_{b_{y}} \\ \nabla \cdot \tilde{\mathbf{R}}_{b_{x}} \end{array} \right] d\Omega \\ &= \frac{1}{|C_{P}|} \iint_{\partial C_{PQ}} \left[\begin{array}{c} \tilde{\mathbf{R}}_{b_{x}} \cdot \tilde{\mathbf{n}} \\ \tilde{\mathbf{R}}_{b_{y}} \cdot \tilde{\mathbf{n}} \end{array} \right] dl \approx \frac{1}{|C_{P}|} \left[\begin{array}{c} \tilde{\mathbf{R}}_{b_{x}} \cdot \mathbf{n}_{PQ} \\ \tilde{\mathbf{R}}_{b_{y}} \cdot \mathbf{n}_{PQ} \end{array} \right]_{M} \end{aligned}$$

$$R_{b_x} = \nabla \cdot \tilde{\mathbf{R}}_{b_x}, \text{ where } \tilde{\mathbf{R}}_{b_x} = \begin{bmatrix} \nu(Hu)_x & \frac{\nu}{2}((Hu)_y + (Hv)_x) \end{bmatrix}^{\mathrm{T}}$$
$$R_{b_y} = \nabla \cdot \tilde{\mathbf{R}}_{b_y}, \text{ where } \tilde{\mathbf{R}}_{b_y} = \begin{bmatrix} \frac{\nu}{2}((Hu)_y + (Hv)_x) & \nu(Hv)_y \end{bmatrix}^{\mathrm{T}}$$

where $\nu = B\delta_b^2 H\eta_t$ is the eddy viscosity coefficient with 0 < B < 1 and δ_b is a mixing length coefficient.



2. Hybrid model

Idea: switching off the dispersive terms.

Boussinesq degenerate into NSWE as dispersive terms become negligible (Tonelli and Petti, 2009 & 2010 for the MS equations).

* Criterion: If $\epsilon = \frac{A}{h} \leq 0.8$, Boussinesq equations are solved otherwise NSWE are solved.

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* Need of a "clever" implementation.

Boundary conditions and internal source function:

• Wall (reflective) boundary condition: $\mathbf{u} \cdot \widetilde{\mathbf{n}} = 0$ for $\mathbf{x} \in \partial \Omega$ By conservation of mass (no loss or gain through the wall)

$$\frac{\partial}{\partial t} \iint_{\Omega} H d\Omega + \int_{\partial \Omega} \left[H \mathbf{u} + \left(\frac{z_a^2}{2} - \frac{h^2}{6} \right) h \nabla (\nabla \cdot \mathbf{u}) + \left(z_a + \frac{h}{2} \right) h \nabla (\nabla \cdot h \mathbf{u}) \right] \cdot \widetilde{\mathbf{n}} dl = 0$$

Define the normal boundary advective flux in weak form, $\Phi_{P,\Gamma} = \begin{bmatrix} 0 \\ \frac{1}{2}g(H^*)^2 n_{P,1x} \\ \frac{1}{2}g(H^*)^2 n_{P,1y} \end{bmatrix}$ by the **method of characteristics**



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Absorbing boundaries: should dissipate the energy of incoming waves
Sponge layer is defined:
$$m(\mathbf{x}) = \sqrt{1 - \left(\frac{\mathbf{x} - d(\mathbf{x})}{L_s}\right)^2}, \ L \le L_s \le 1.5L,$$

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- Internal source function for regular waves (Wei et al., 1993) added to the mass equation

$$S(\mathbf{x},t) = D^* \exp\left(\gamma (x - x_s)^2\right) \sin(\lambda y - \omega t)$$

Area: $(x, y) = [-5, 28m] \times [0, 30m], A/h = 0.18, N = 52, 191, CFL = 0.8$ Using mesh h- enrichment



















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2D run-up of a solitary wave on a conical island (cont)

Time series of surface elevation at wave gauges around the island:



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Experimental measurements and numerical runup around the conical island:



Simulation \sim 28min on a single 2.4GHz Intel Core 2 Quad Q6600 processor

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II. Wave propagation over a semicircular shoal (Whalin, 1971)

Case B: T = 2.0s, h/L = 0.117, A/h = 0.0165, kh = 0.735 and S = 1.198

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Free surface and spatial evolution of the 1st, 2nd and 3rd harmonic

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III. Breaking on a sloping beach (Hansen and Svendsen, 1979)

Area: $(x, y) = [-26, 26m] \times [0, 1m], \ N = 24,996$, CFL = 0.4

Case B (Spilling-plunging): T = 2.5s, H = 0.39m, S = 8.6032



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Breaking on a sloping beach

Case C (Spilling): T = 2.0s, H = 0.36m, S = 4.8077



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IV. Wave over a bar (Beji and Battjes, 1993)

 $(x,y) = [-10, 30m] \times [0, 0.8m], H = 0.02m, T = 2.02s, N = 40, 364, CFL = 0.4$



IV. Wave over a bar (Beji and Battjes, 1993)

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Area: $(x, y) = [0, 83m] \times [0, 1m], A/h = 0.3, N = 10,900, CFL = 0.4, n_m = 0.014$ —Hybrid and — Eddy viscosity



Shoaling, before breaking

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Two-dimensional reef (cont.)



Hydraulic jump on the fore reef

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Two-dimensional reef (cont.)



Hydraulic jump on the fore reef

26

Two-dimensional reef (cont.)



Hydraulic jump on the fore reef

Time series of surface elevation at wave gauges:









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Time series of surface elevation at wave gauges:



Time series of surface elevation at wave gauges:



Time series of surface elevation at wave gauges:



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Time series of surface elevation at wave gauges:



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Time series of velocities at wave gauges:



Time series of velocities at wave gauges:



Time series of velocities at wave gauges:



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Time series of velocities at wave gauges:





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- Two different types of **wave breaking** mechanisms are implement with comparable performance.
- Relatively straight forward to **extend existing NSWE codes** that use (unstructured) FV schemes as to include dispersion characteristics for deeper water simulations.

Thank you for your attention!!

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2D solitary wave propagation in a channel

Area: $(x, y) = [-100, 2400m] \times [-5, 5m], A/h = 0.2, N = 53, 304, CFL = 0.8.$
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Area: $(x, y) = [-4, 10m] \times [-0, 0.55m], A/h = 0.25, N = 10,609, CFL = 0.8$ Use of an h- enrichment technique (Nikolos and Delis, 2009)



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Solitary wave-cylinder interaction: numerical and experimental results for η at WG1-WG6



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